Green Water Events: Features and Related Hydrodynamic Phenomena



Konstruksjonsdagen 2025



Green Water involves compact masses of water entering decks/compartments of ships or marine structures, which are exposed to the external waves.

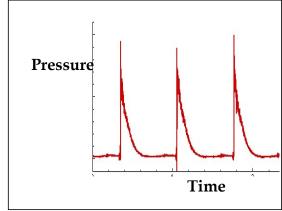
Issues: Safety, Operations, Costs

Green Water - 3 Driving Research Questions

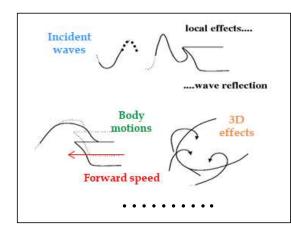
1. What are the most common and the most critical Green-Water Scenarios?



2. What are the Green-Water Loads and how they can be dangerous?

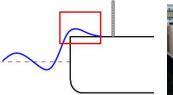


3. Which Wave-Body Parameters and Physics matter for Green Water and for its Consequences?



Green Water - Study Cases

 2D & 3D studies relevant for FPSOs (fixed/free-floating) in head-sea waves

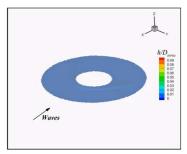






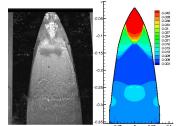
 3D study on a non-ship shaped renewable-energy concept in waves



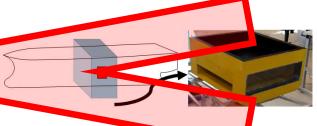


 3D study on a ship (w/o and with forward speed) in head & nearly head-sea waves



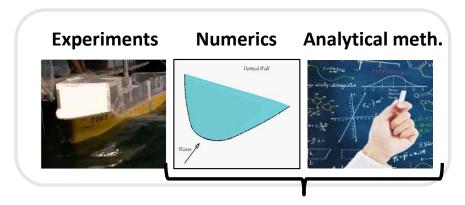


 2D study on a damaged midship section in beam-sea waves

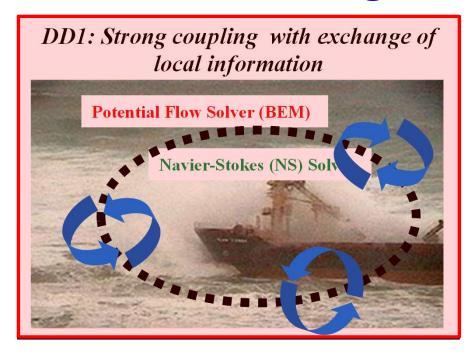




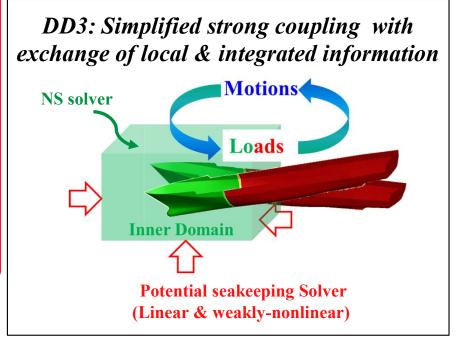
Green Water - Research Tools & Strategies



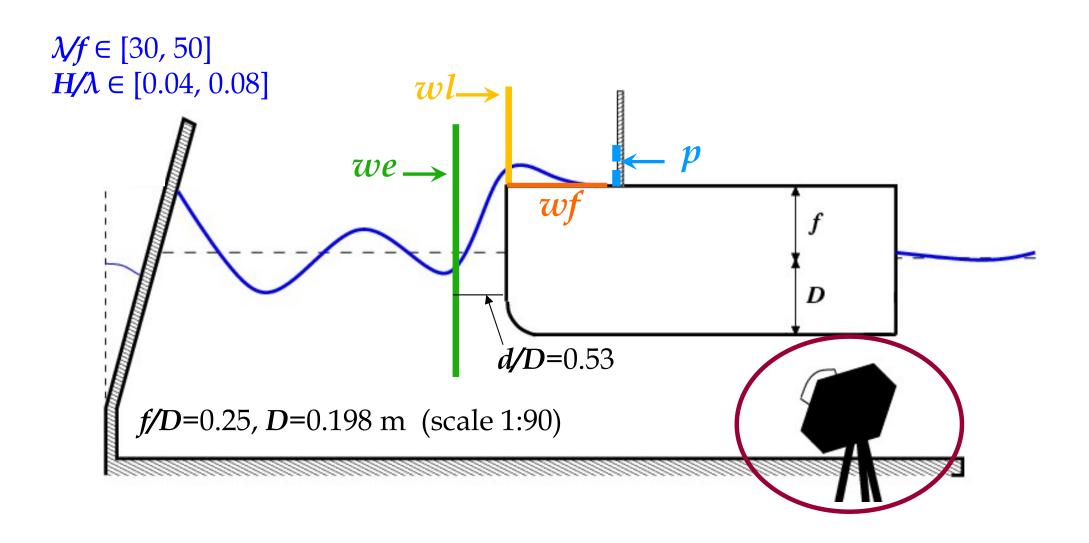
- > Potential flow solver (BEM)
- > Domain Decompositions (DD) Strategies





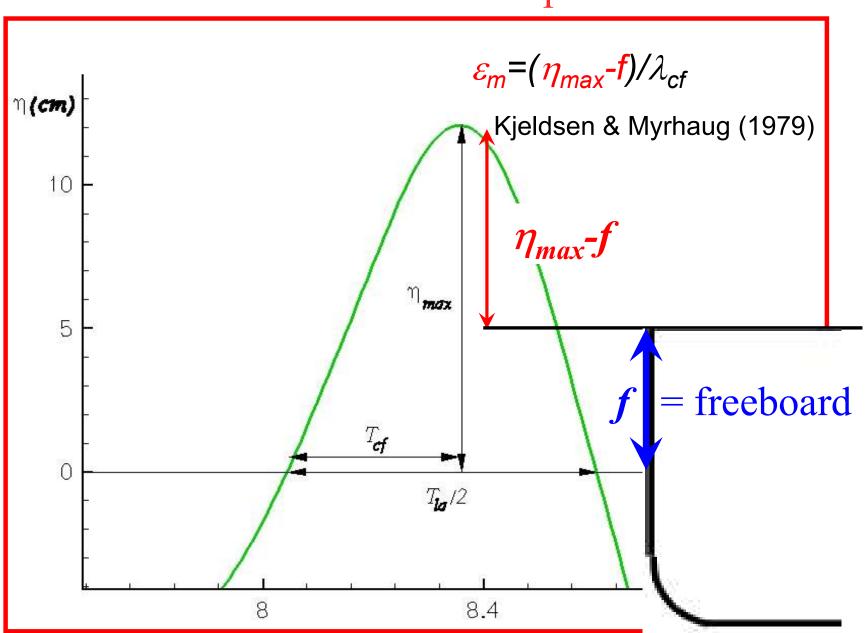


2D Water-on-Deck Experiments

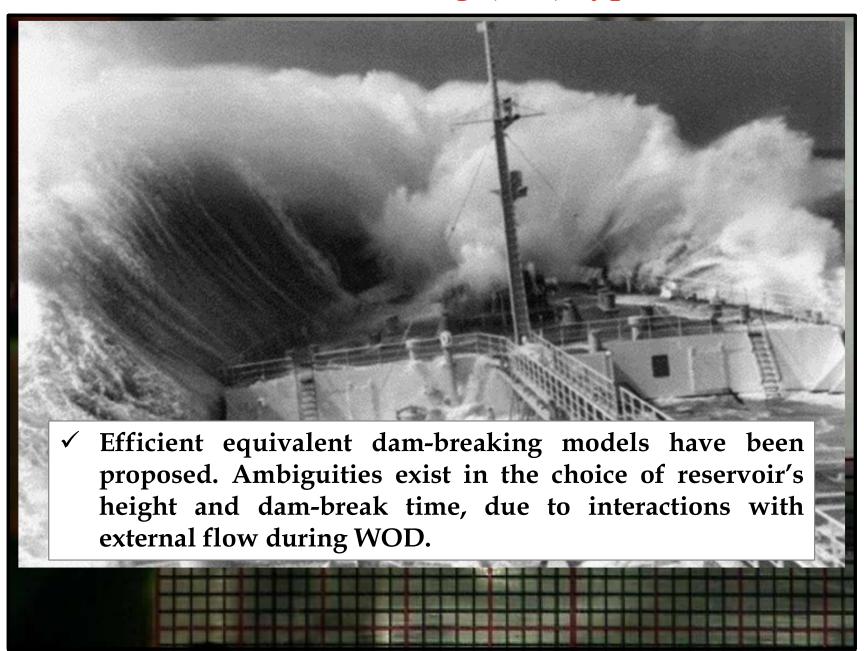


Incoming Wave 'Definition'

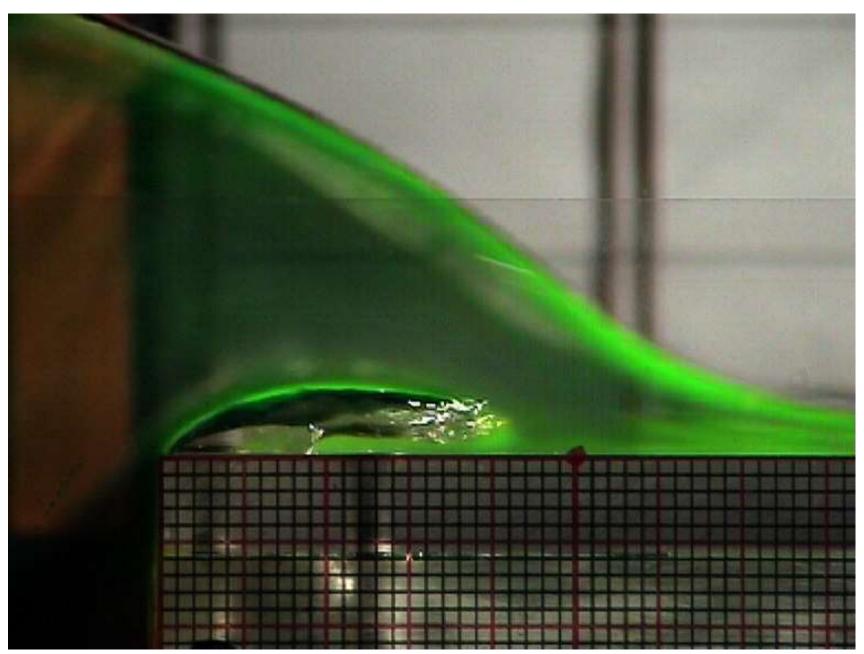
Crest-front local steepness



Dam-Breaking (DB) type

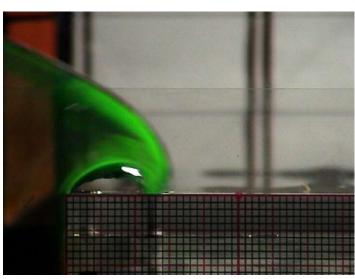


Plunging-Wave (PW) type



Plunging-Wave plus Dam-Breaking (PDB) type

PDB type



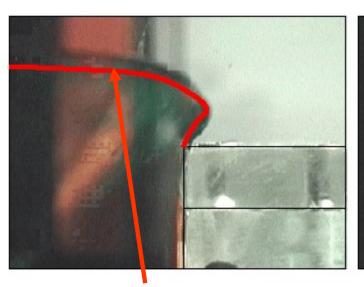
Initial stages

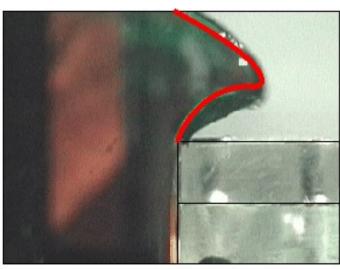


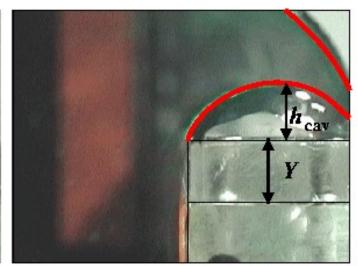
Later stages

Plunging Phase

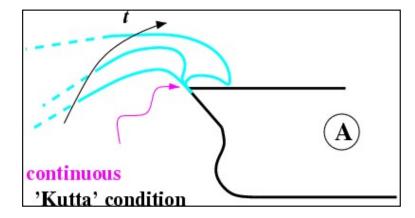
Time



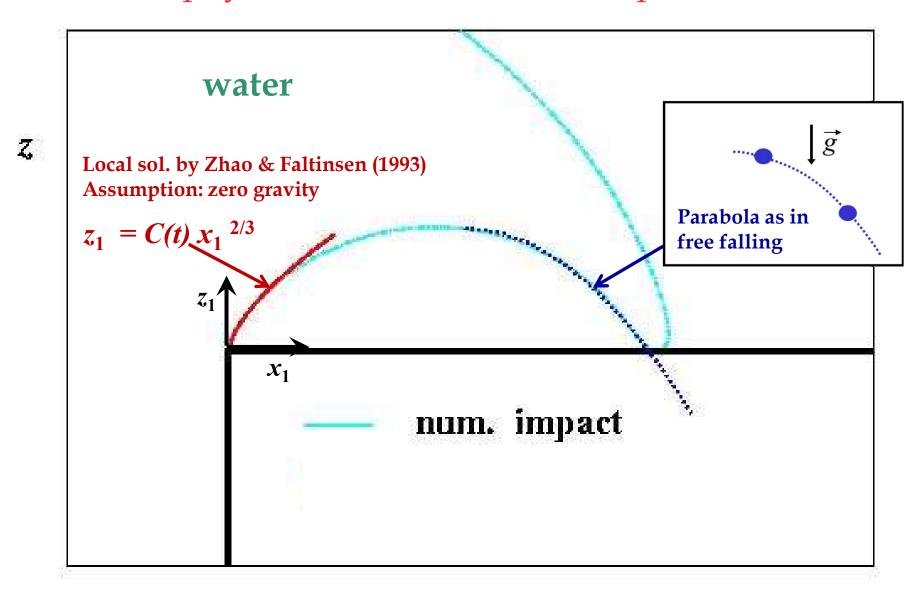




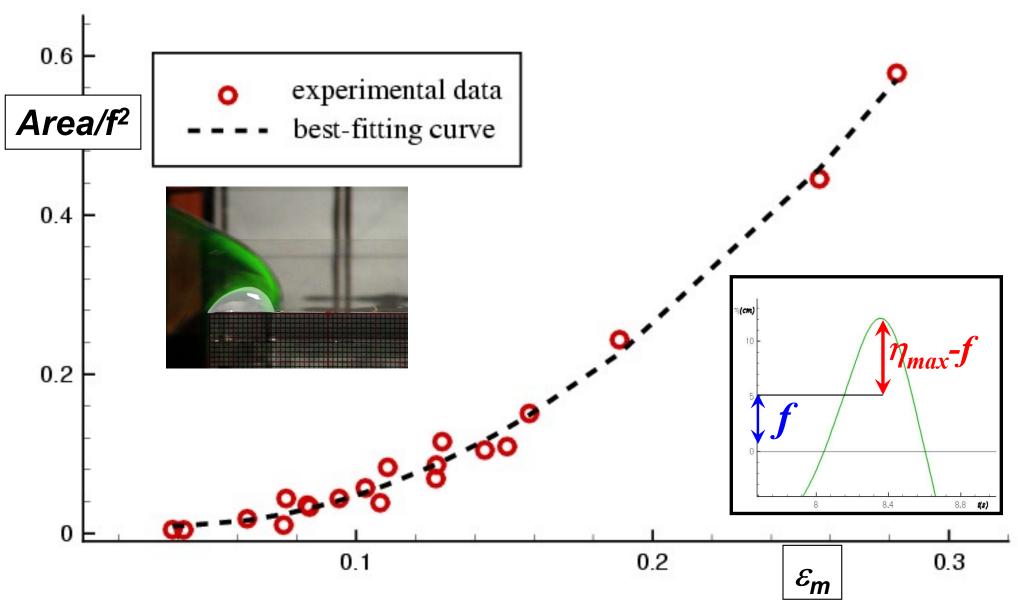
BEM Results



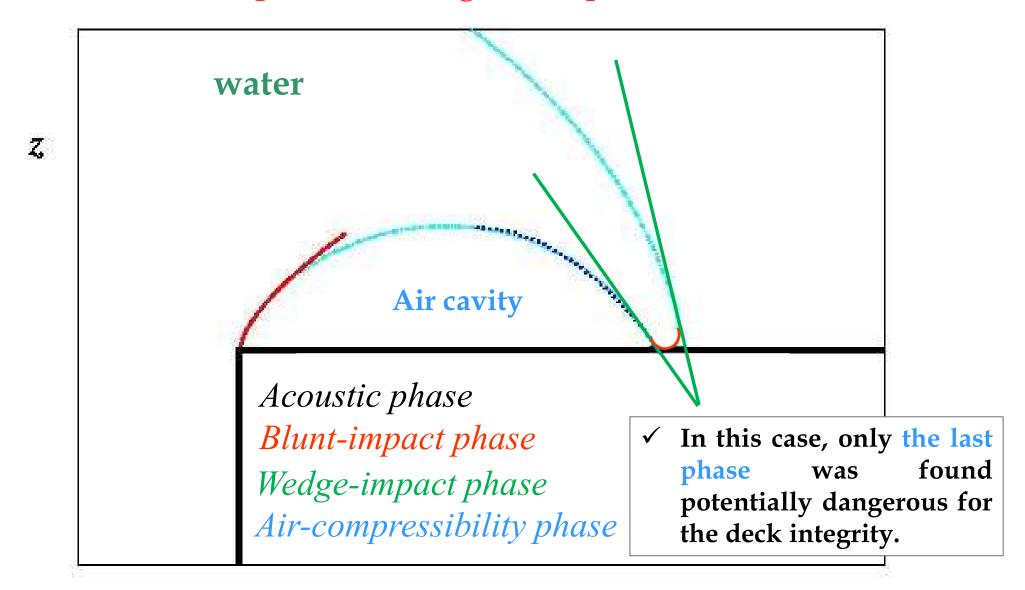
Relevant physical effects before the impact with the deck

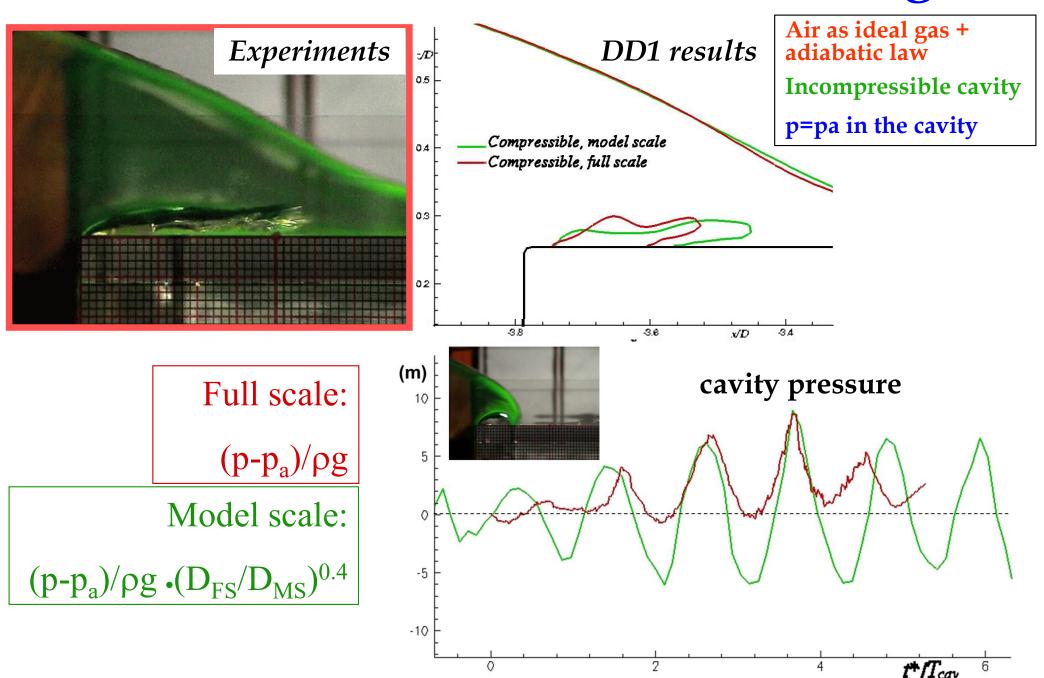


Initial area of the entrapped cavity

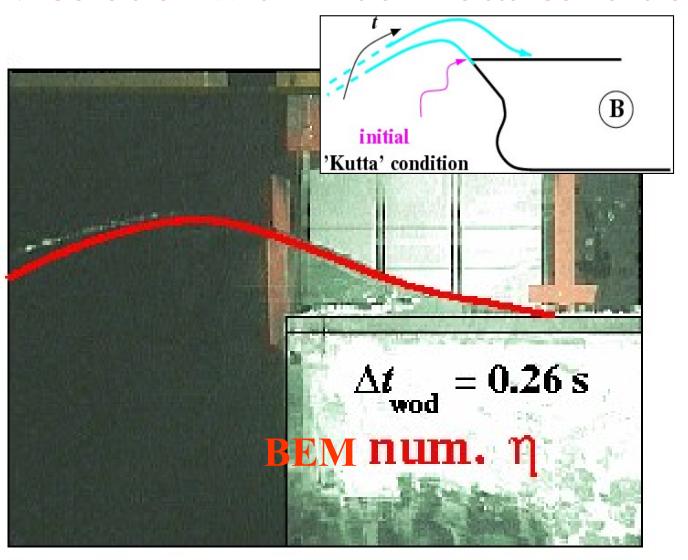


Relevant phases during the impact with the deck

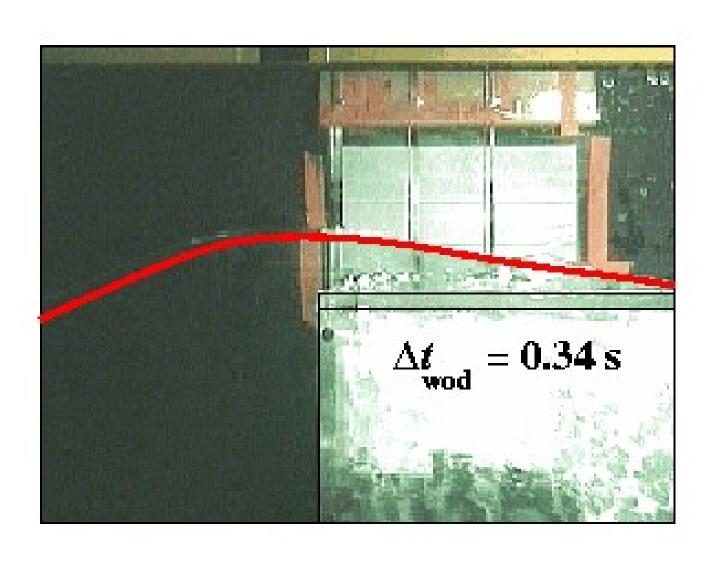




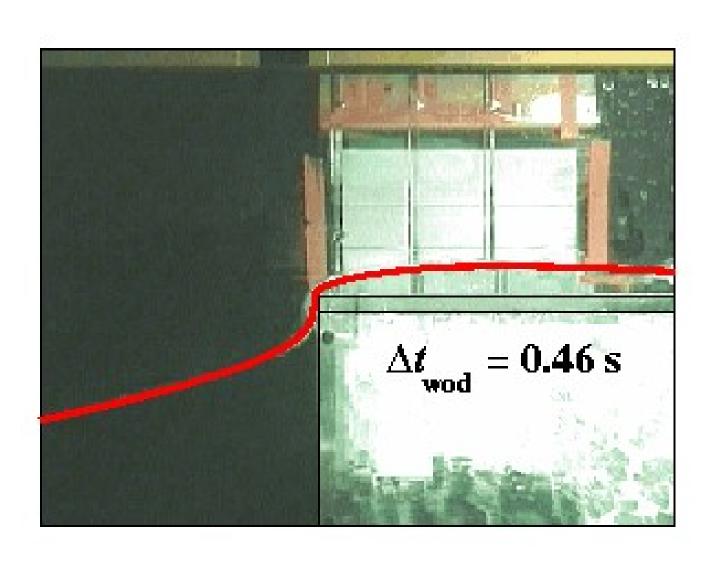
BEM solution with Initial-Kutta condition



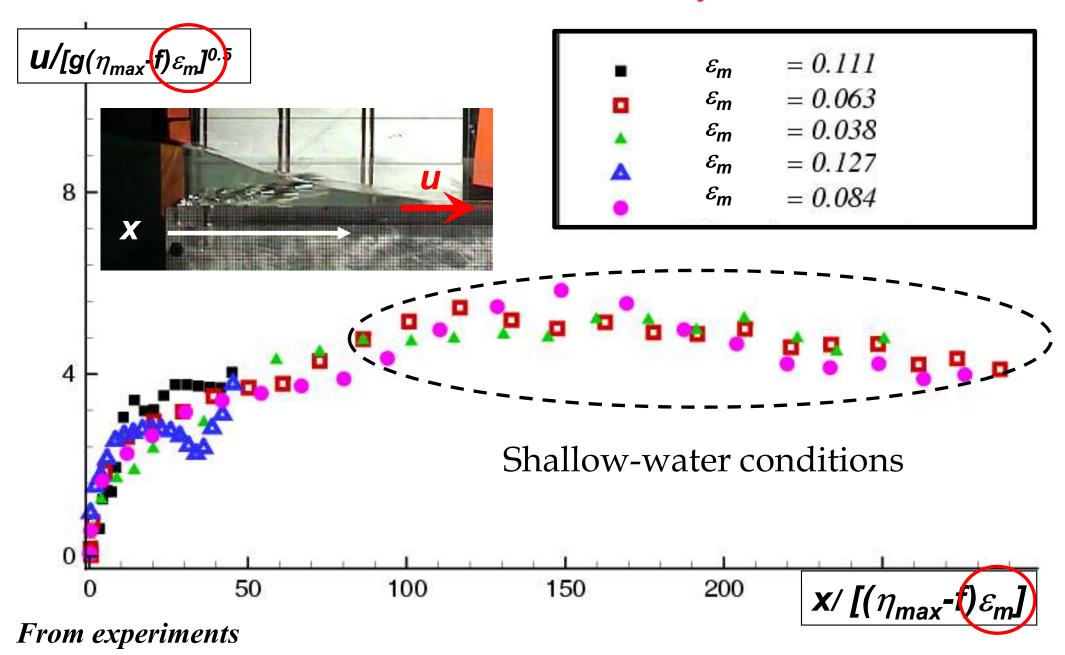
BEM solution with Initial-Kutta condition



BEM solution with Initial-Kutta condition



Water-front velocity



Flow evolution and interaction with a superstructure



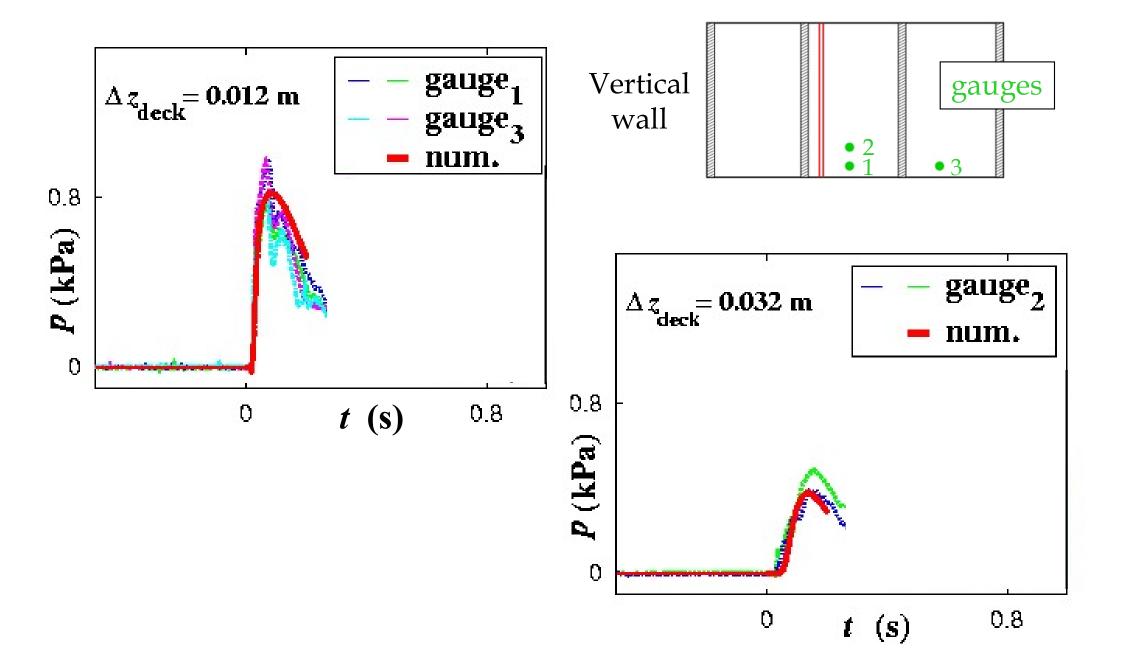
PDB Water-on-Deck: Later stages Flow evolution and interaction with a superstructure



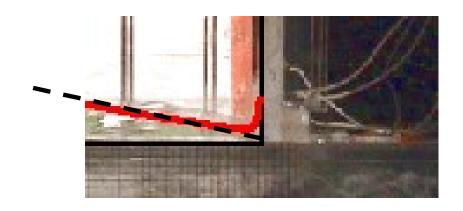
PDB Water-on-Deck: Later stages Flow evolution and interaction with a superstructure



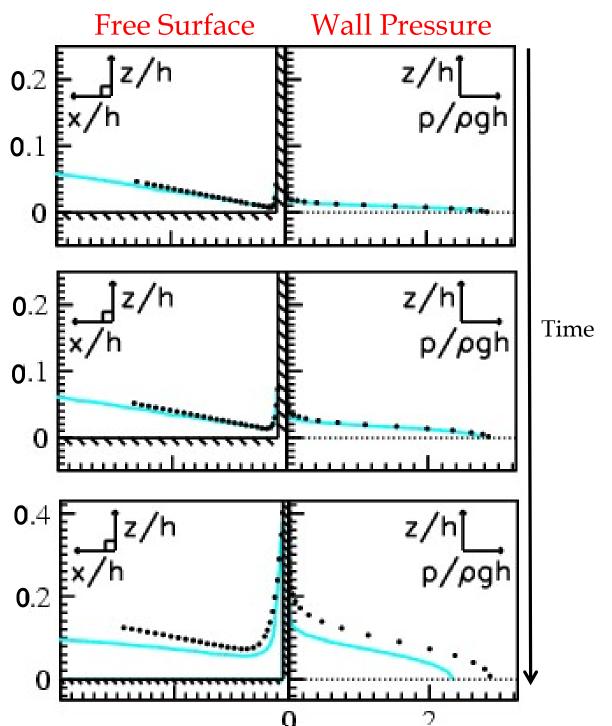
Impact with a Vertical Superstructure Experimental and BEM Pressure along the Wall



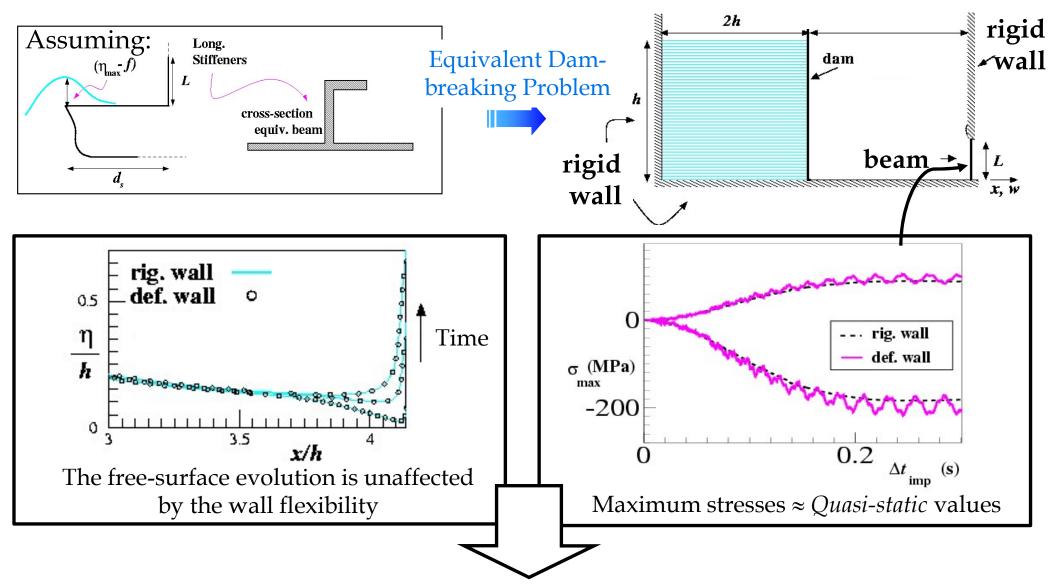
Initial Impact with Vertical Wall



- BEM sol. (with-gravity)
- zero-gravity sol. Ref.: Zhang *et al.* (1996)
- ✓ As time goes on, gravity slows down the water riseup and limits the pressure.



Hydroelasticity analysis



✓ Limited Role of Hydroelasticity for this WOD Scenario.

From calculations

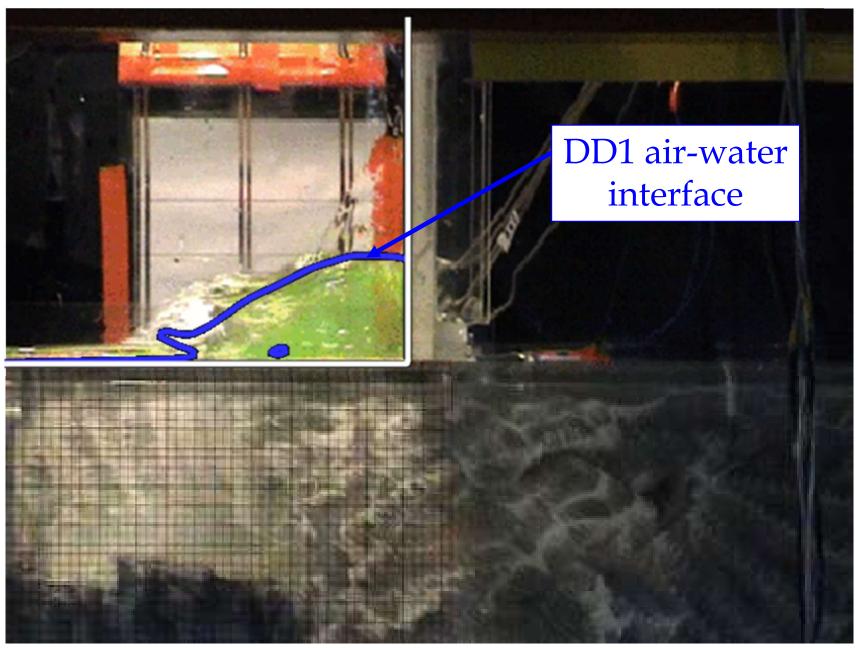
Water Overturning and Breaking



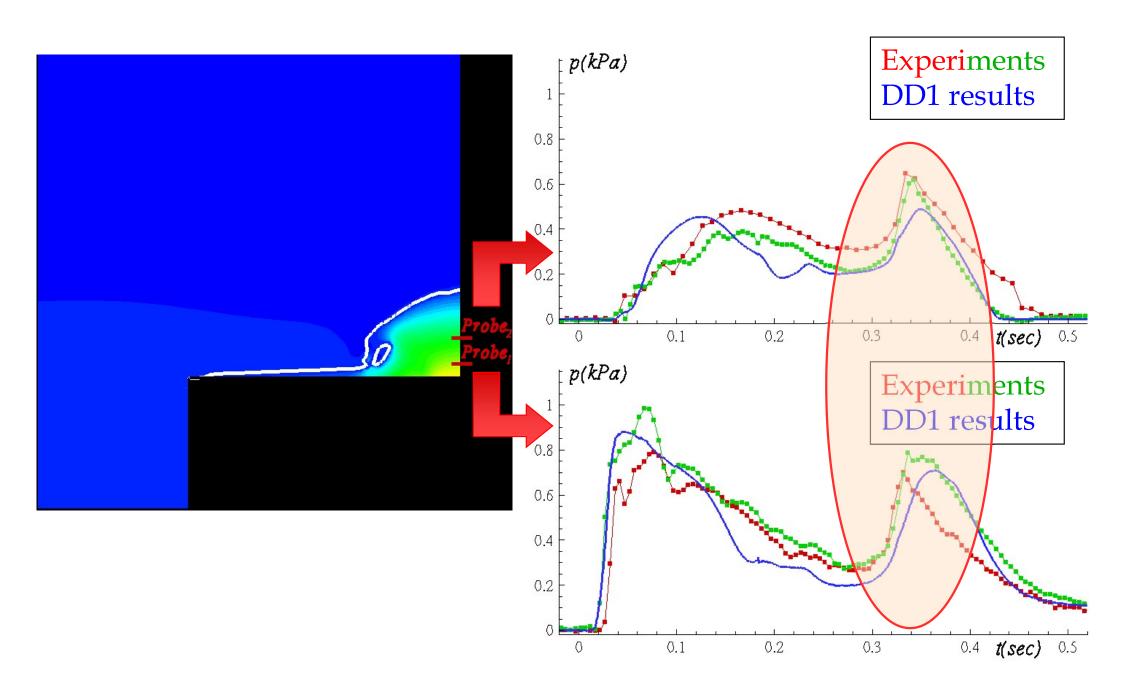
Water Overturning and Breaking



Water Overturning and Breaking

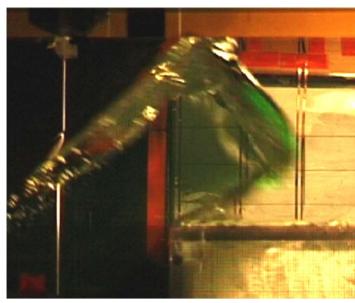


Pressure on the wall: DD1 versus experiments



Hammer-Fist (HF) type

HF type

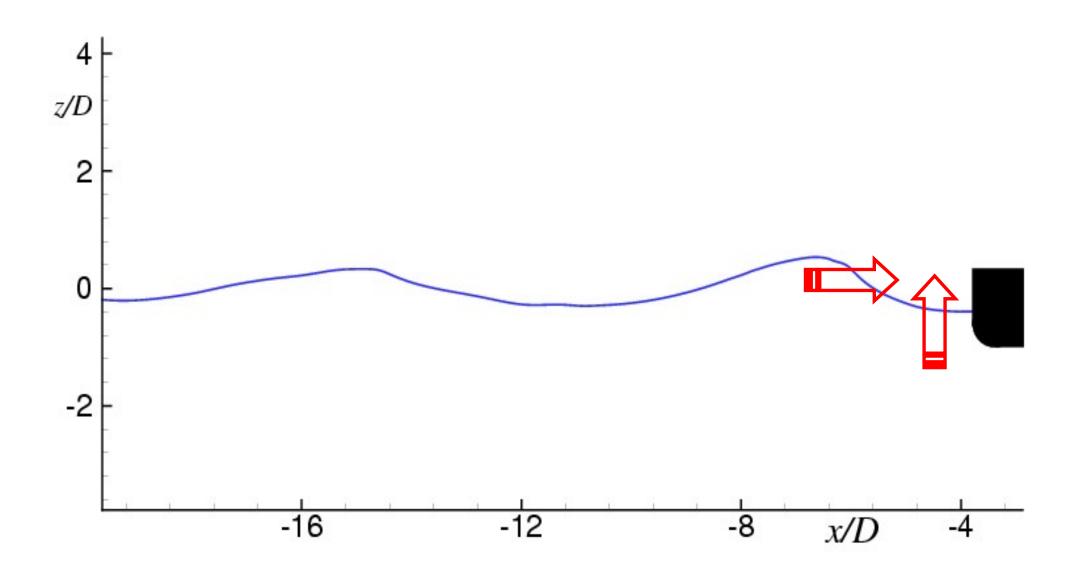


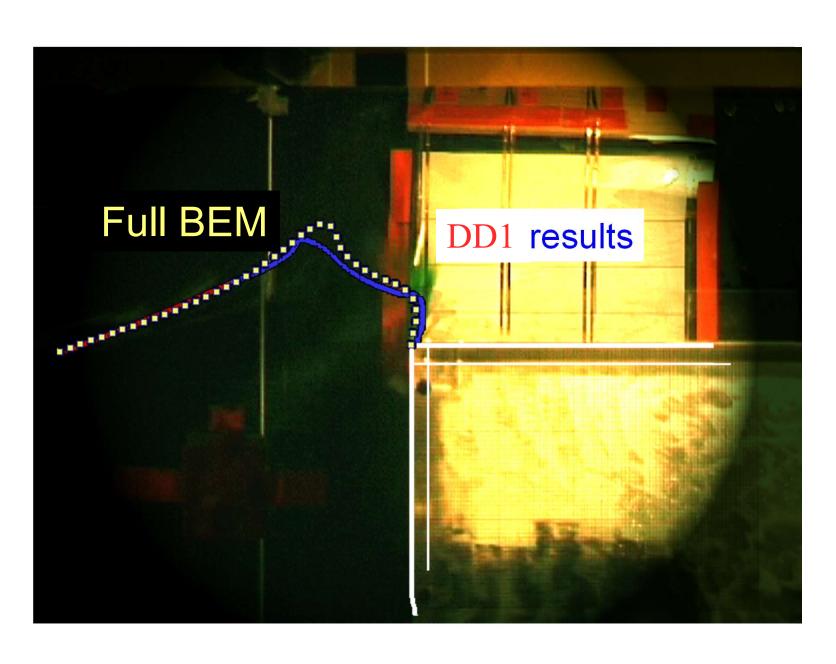




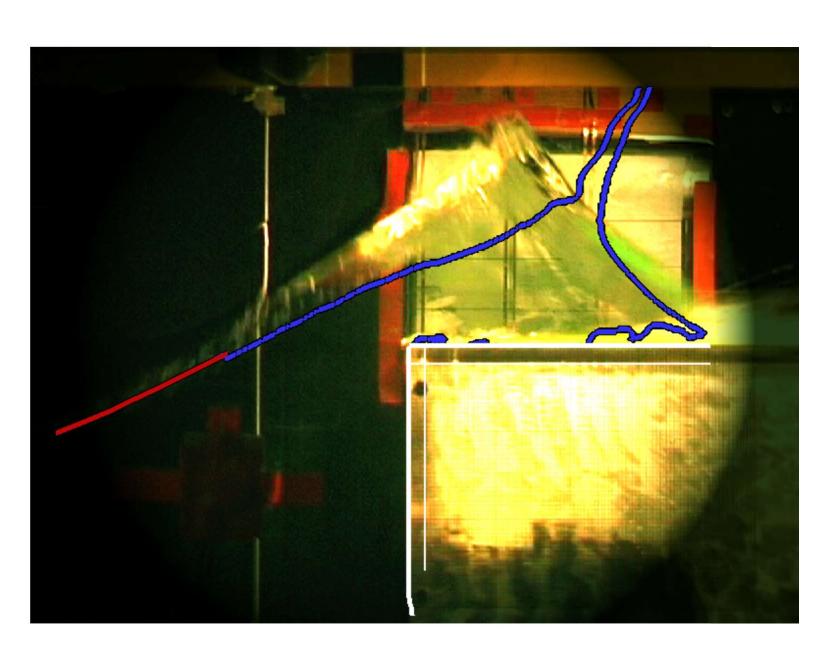


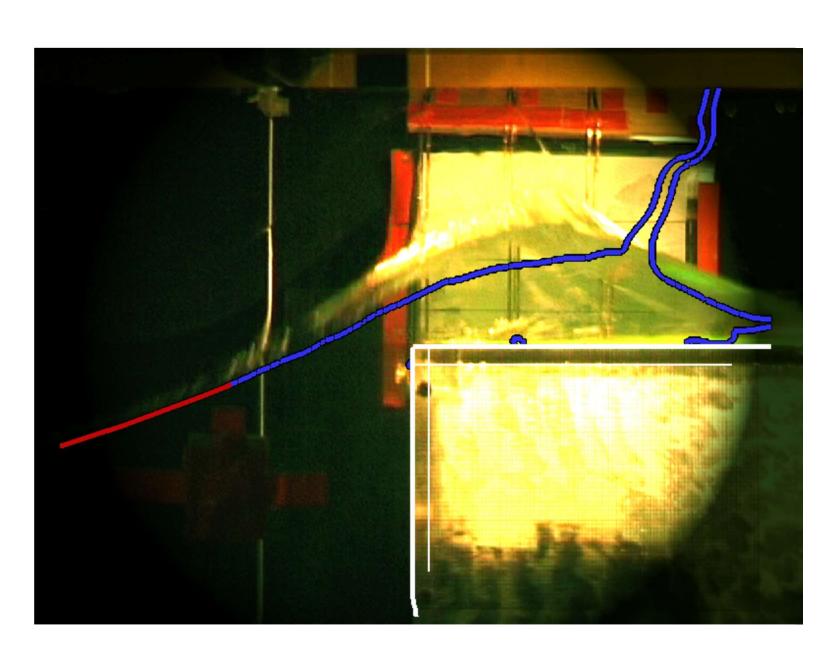
HF Water -on-Deck: Occurrence





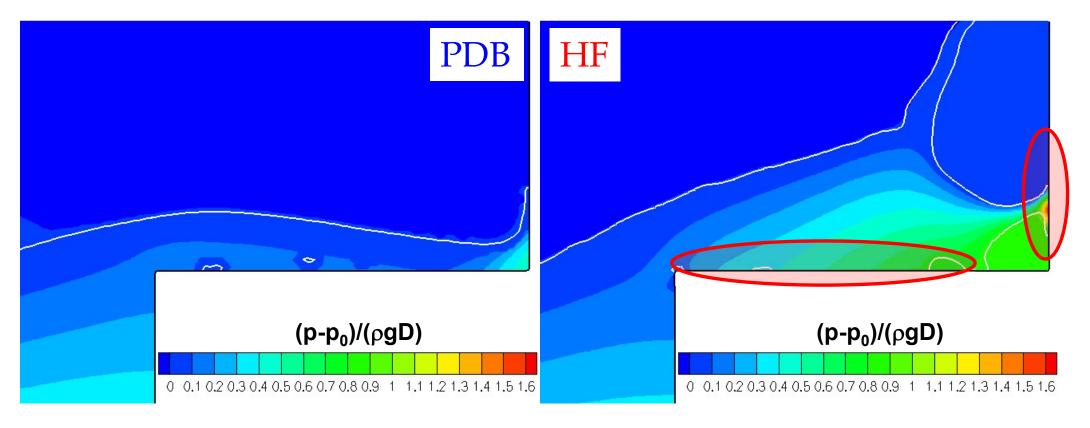






Green-Water Loads: PDB versus HF

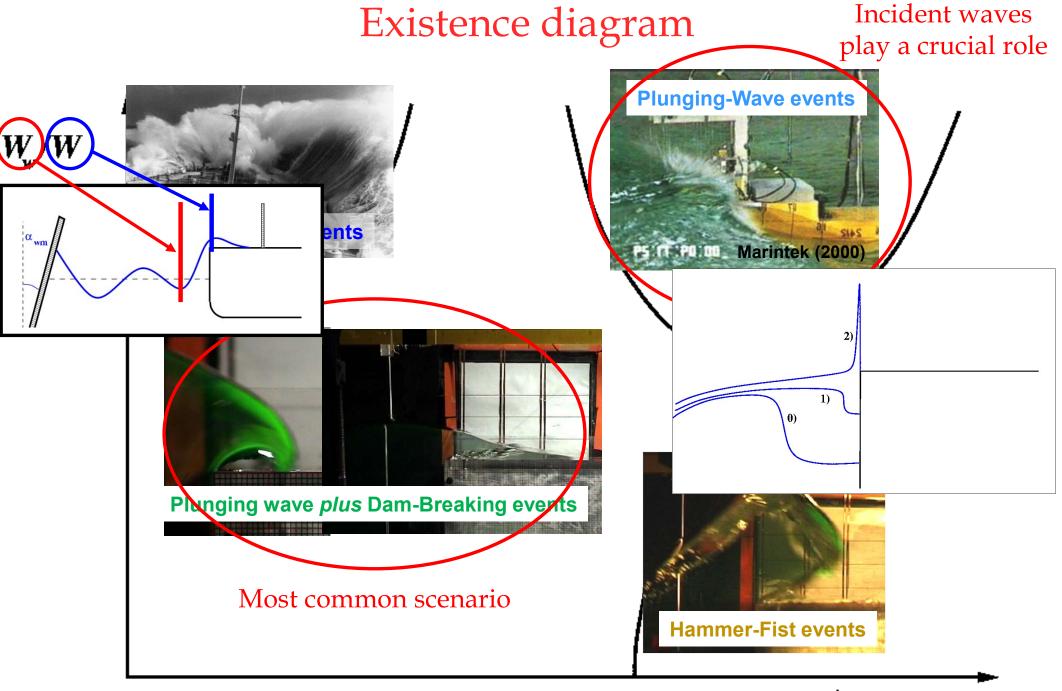
Pressure



- ✓ HF can result in higher over pressures, dangerous for local structural integrity.
- ✓ **HF** can leads to blunt deck impact (with air entrainment) and wall impact not from the foot, both potential risk for hydroelastic excitation. We did not examine this.

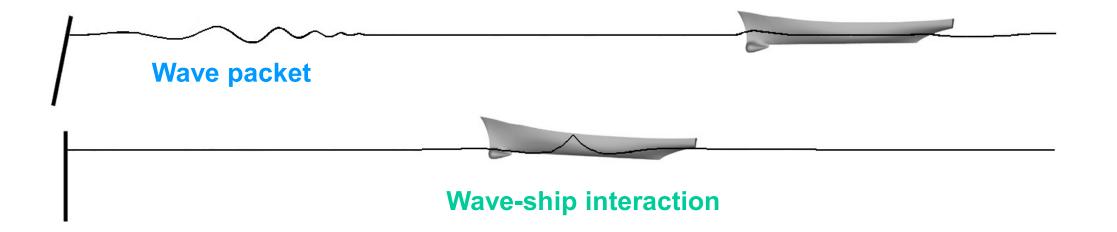
From calculations

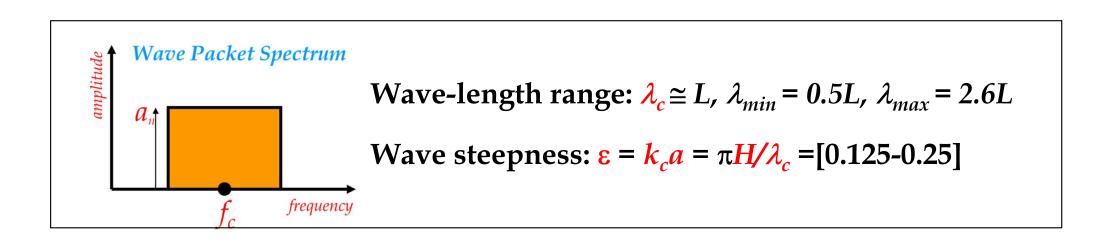
Water-on-Deck Scenarios



3D Model Tests

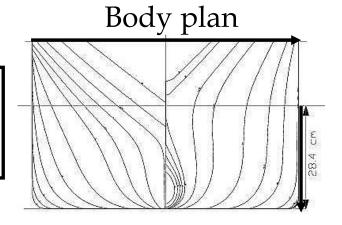
Water on deck in head sea conditions



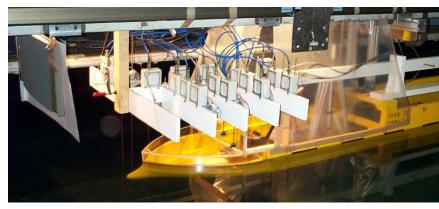


Esso Osaka

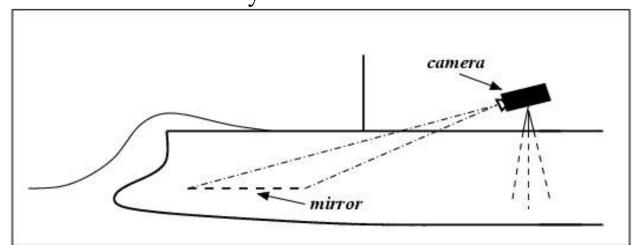
 $L \sim 4.44 \text{ m (scale 1:70)}$ $D/L \sim 0.064, f/L \sim 0.015$ $B/L \sim 0.166, ds/L \sim 0.13$



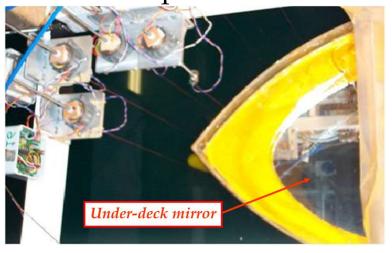
Side view

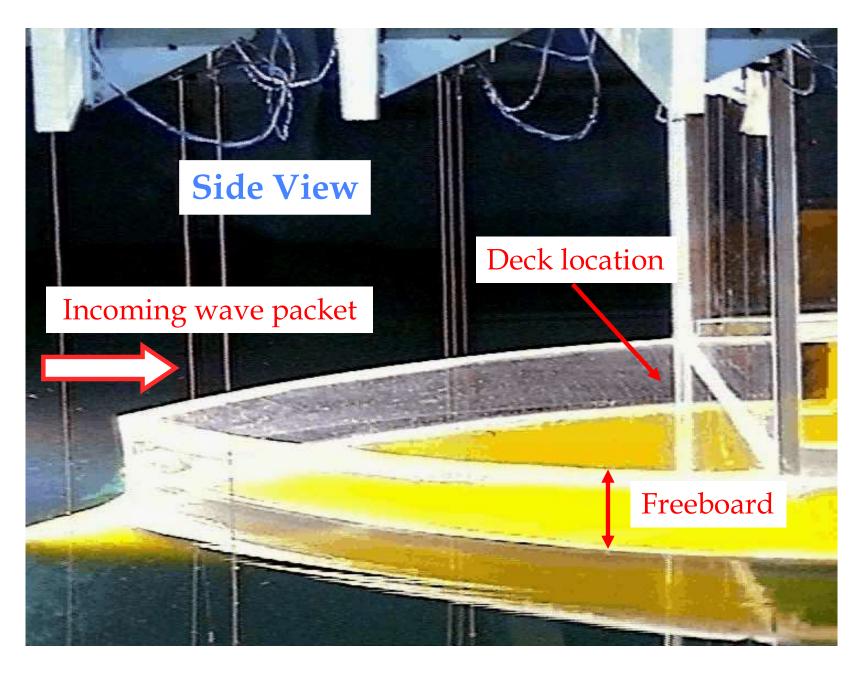


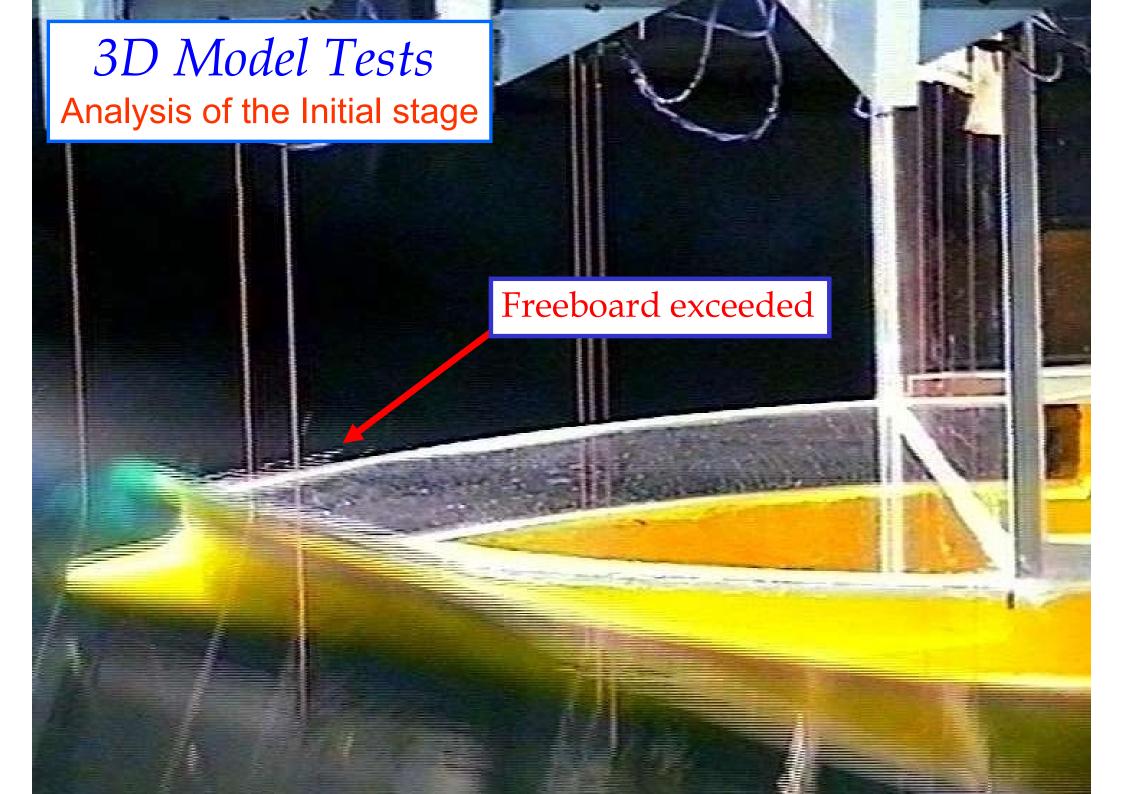
Mirror-camera system: side view sketch

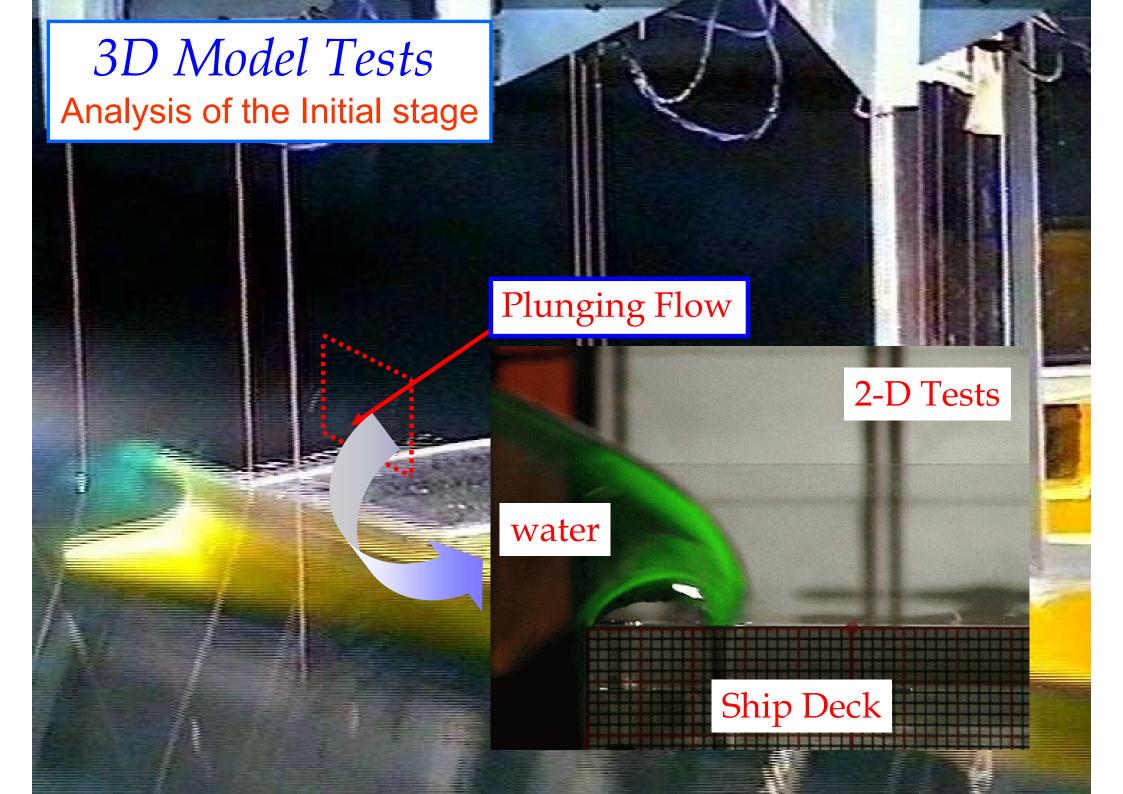


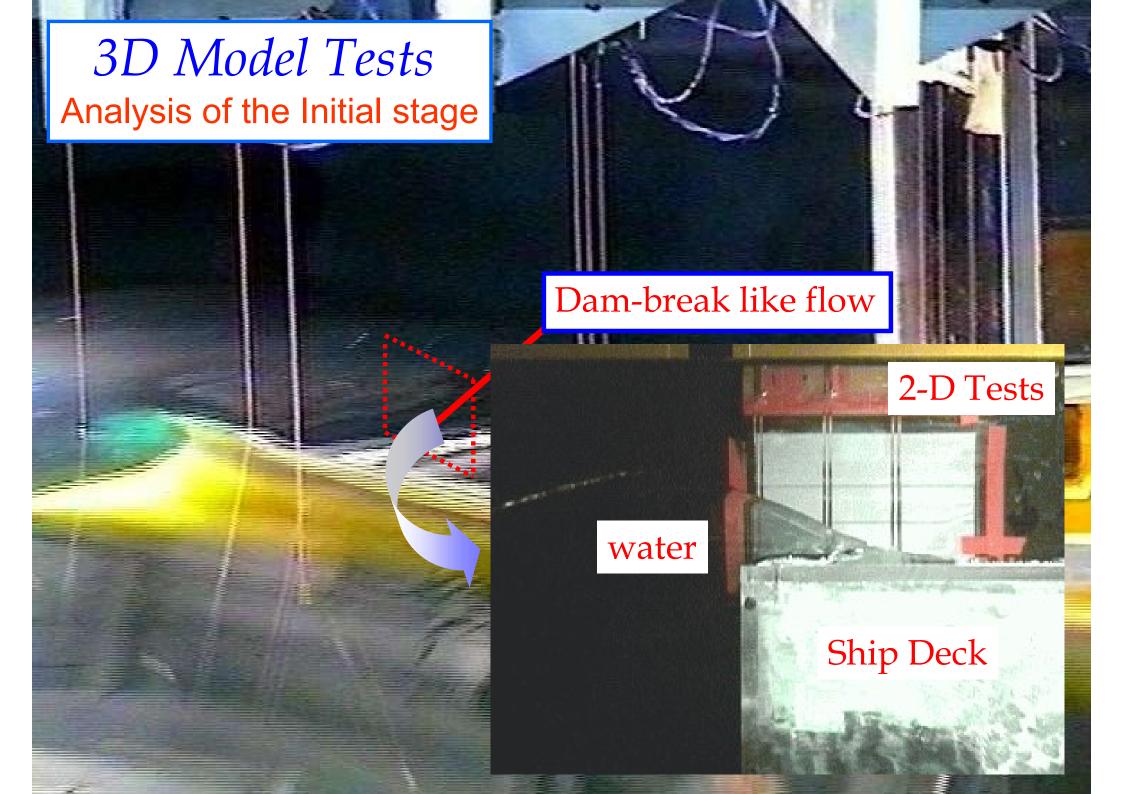
Top view

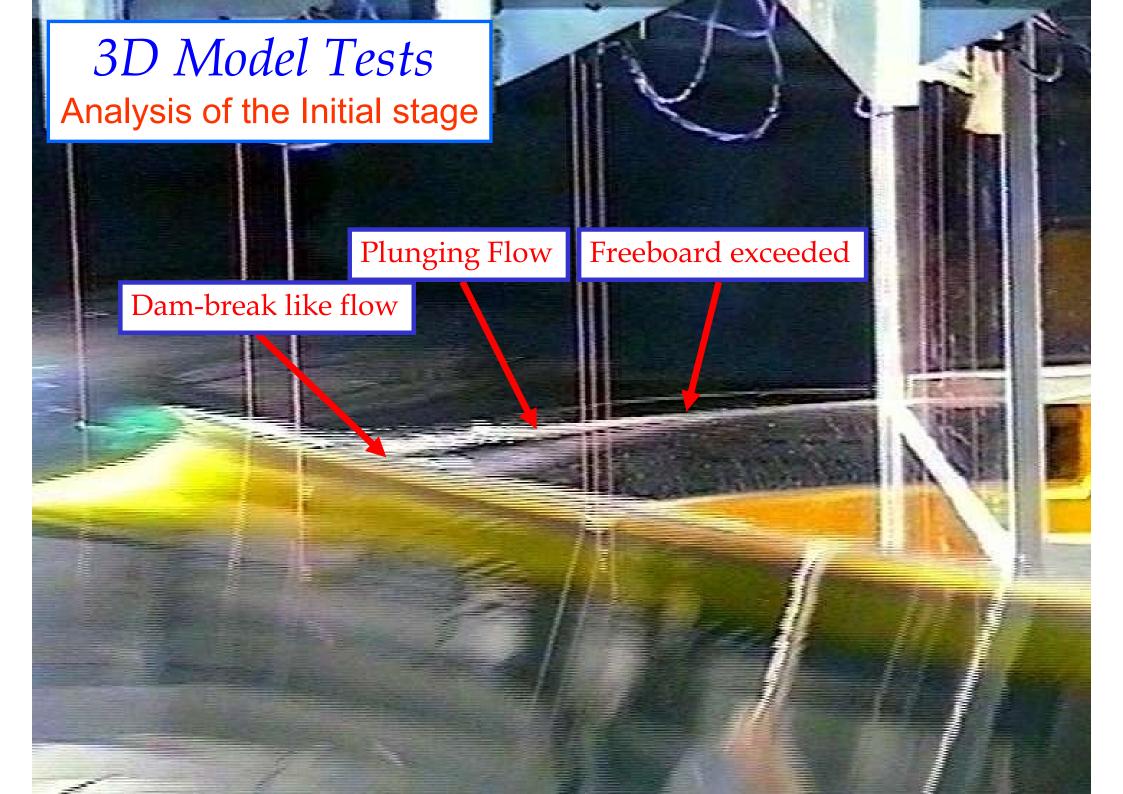






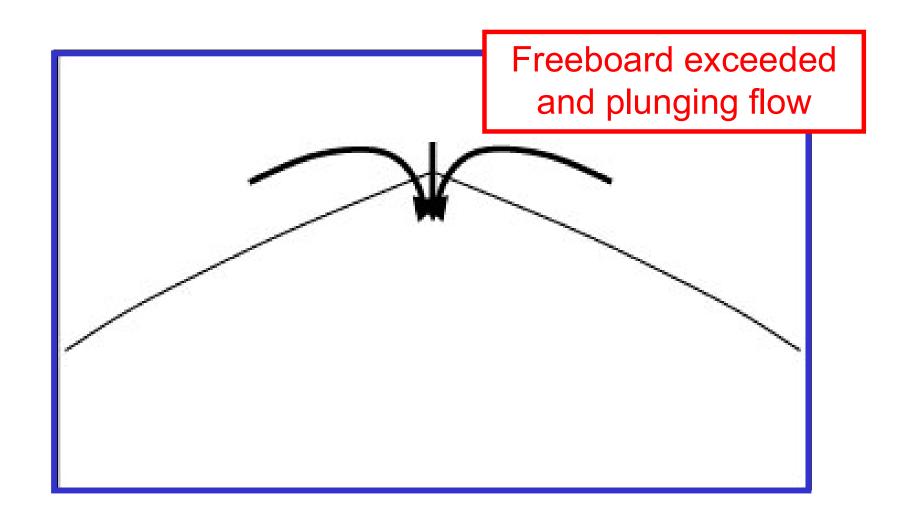




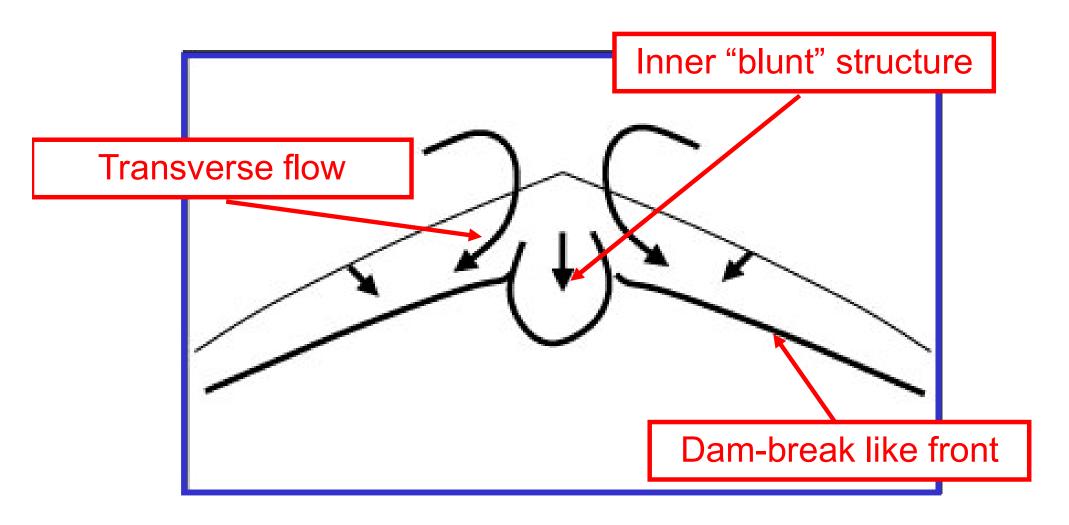


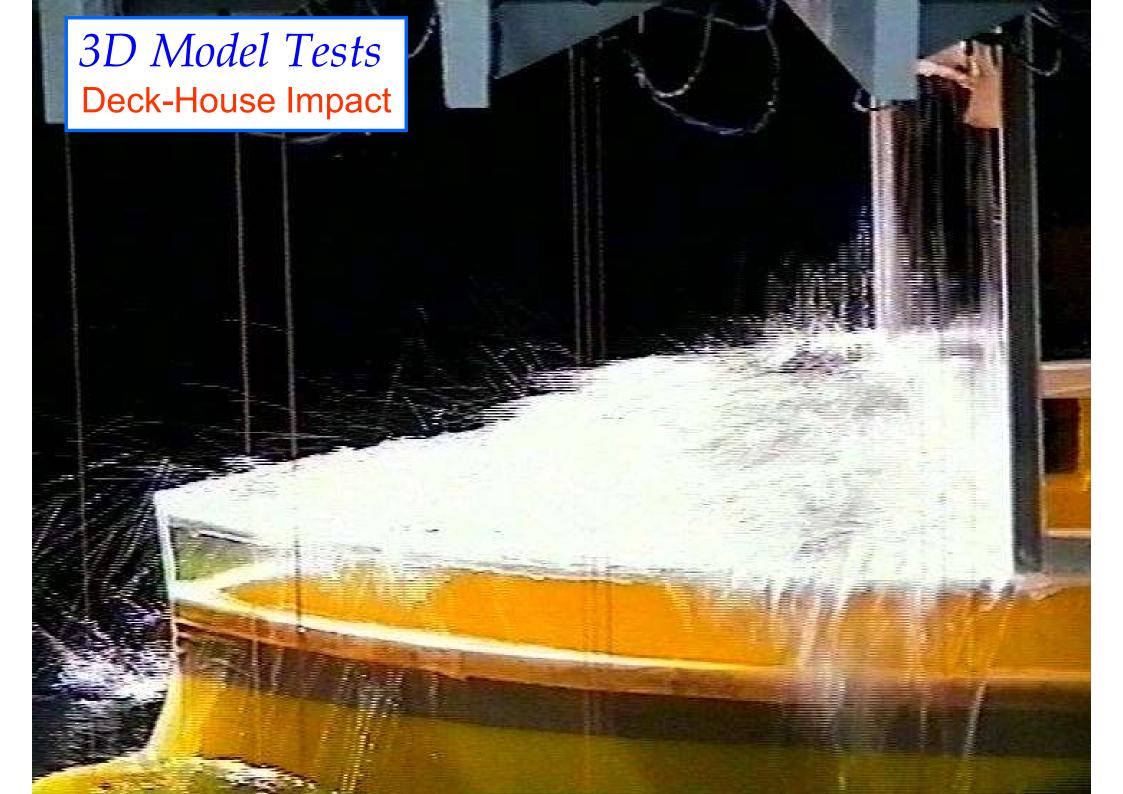


Structure of the deck flow



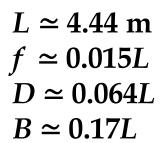
Structure of the deck flow





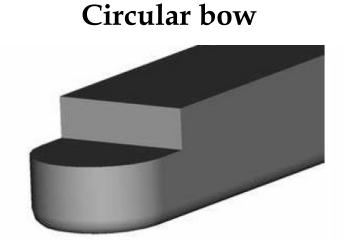
Influence of bow shape

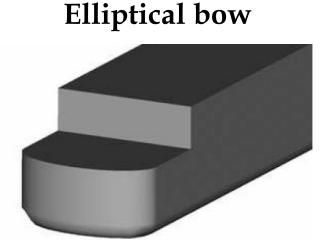
Esso Osaka



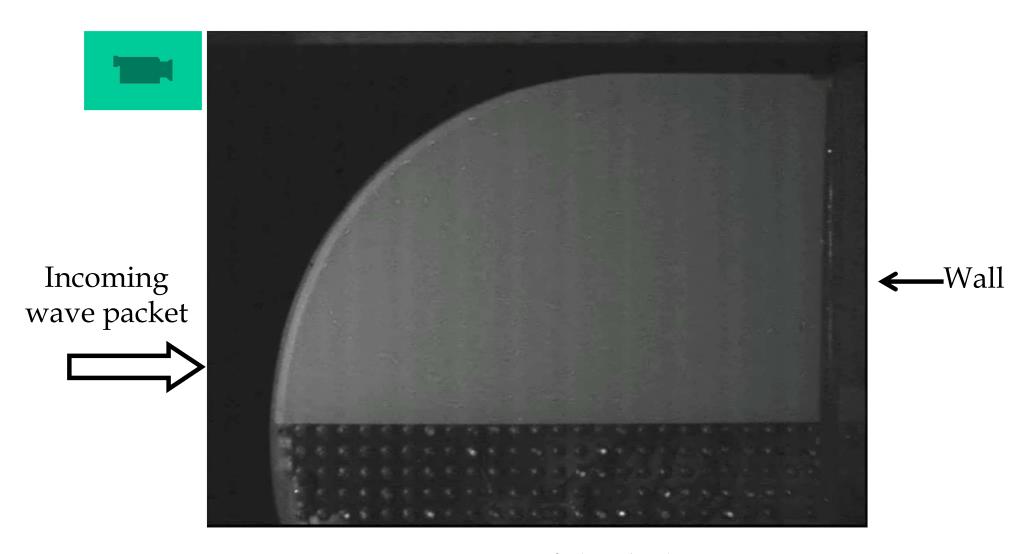


 $L \simeq 4 \text{ m}$ $f \simeq 0.016L$ $D \simeq 0.07L$ $B \simeq 0.17L$



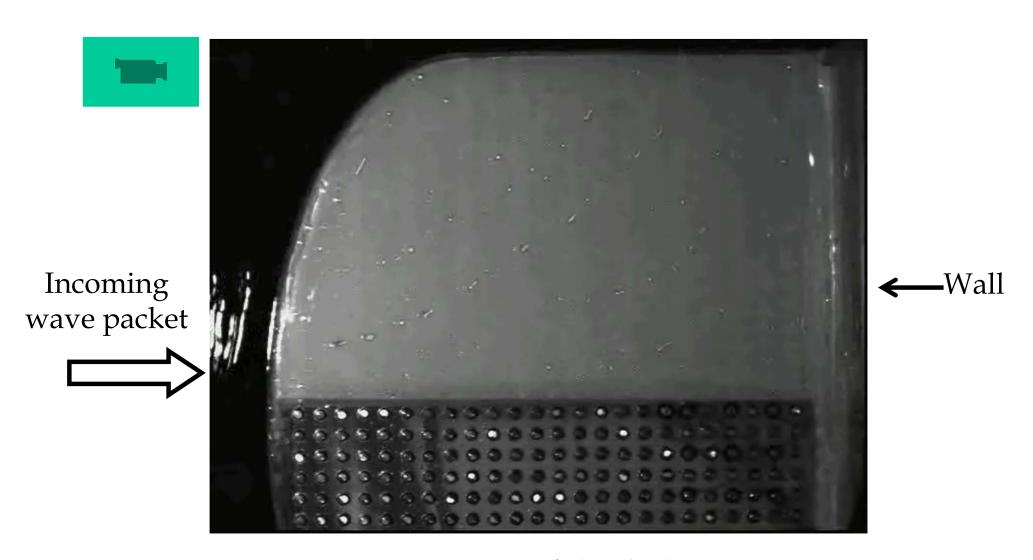


Influence of bow shape: Circular bow



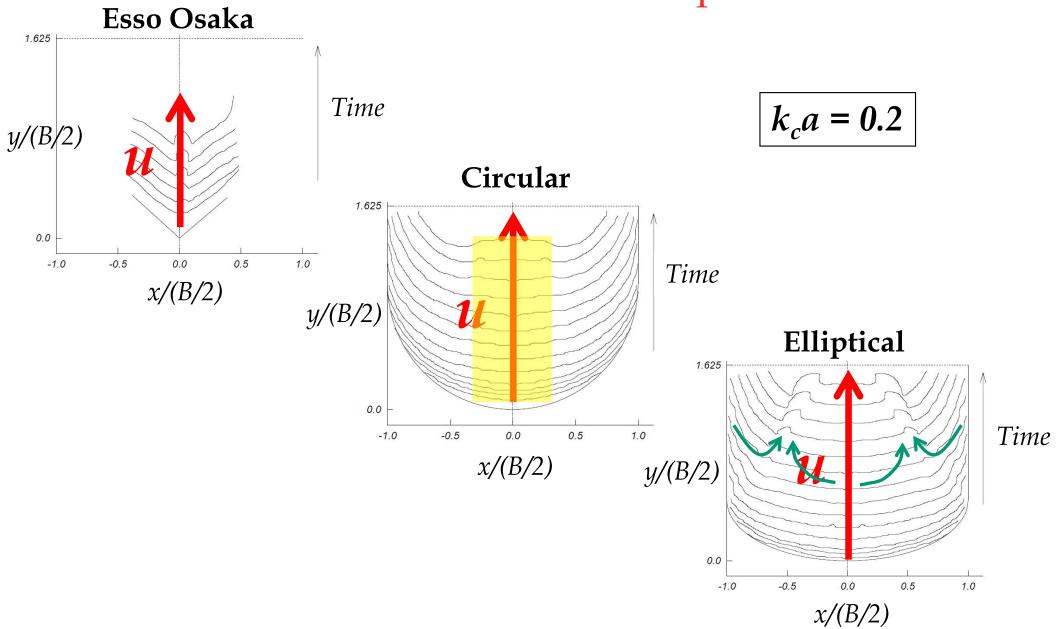
Top view of the deck

Influence of bow shape: Elliptic bow

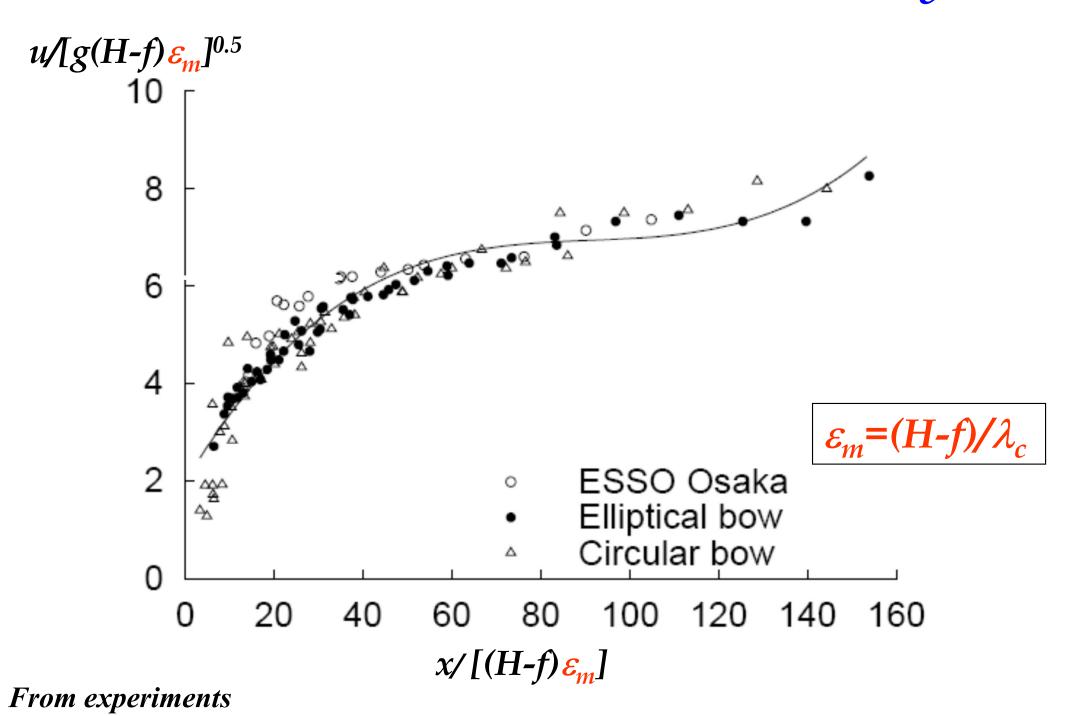


Top view of the deck

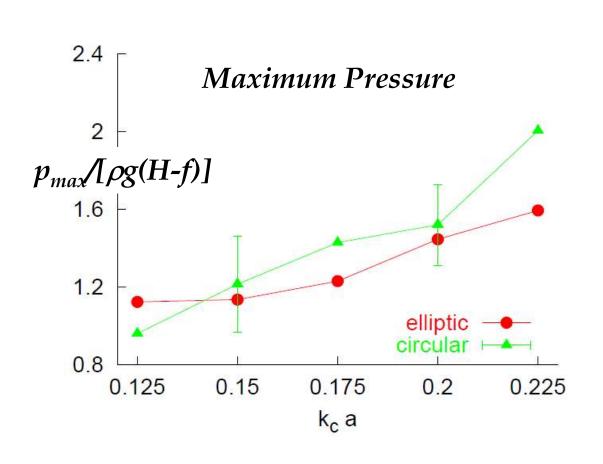
Influence of bow shape



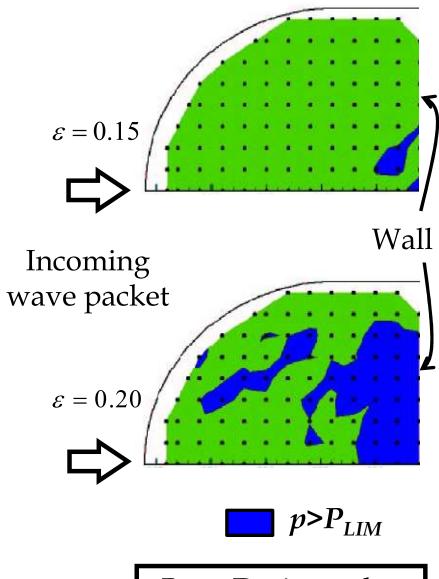
Centreline Water-Front Velocity



Pressure on the Deck

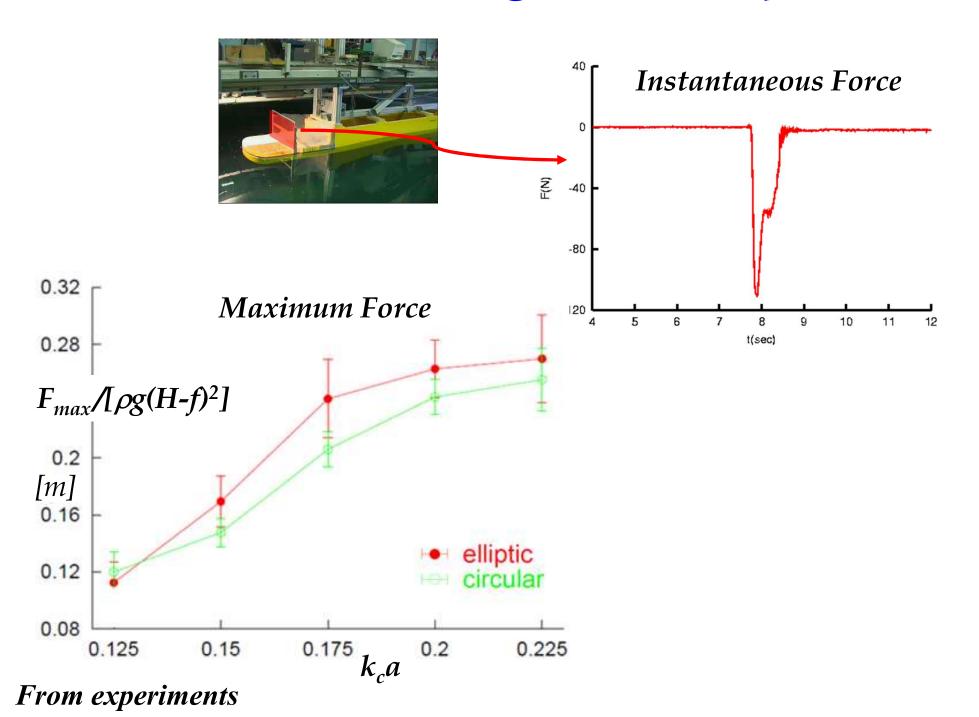


Instantaneous Pressure



 P_{LIM} : Design value

Green-Water Loading on the Superstructure



Green Water and Dynamic Response: a FPSO

FPSO prescribed to be free in heave, pitch and roll.

Regular head-sea waves with A=a=H/2, $\lambda=2\pi/k$, $T=2\pi/\omega$

Front view





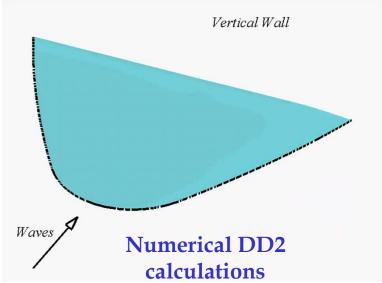
Side view

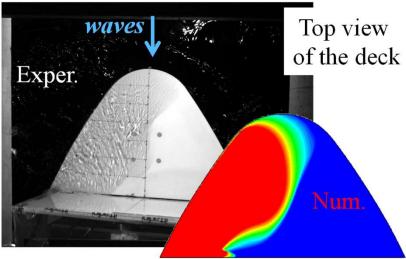
Green water (WPD) & Parametric Roll (PR)

✓ Parametric roll and green water affect, and can cause, each other

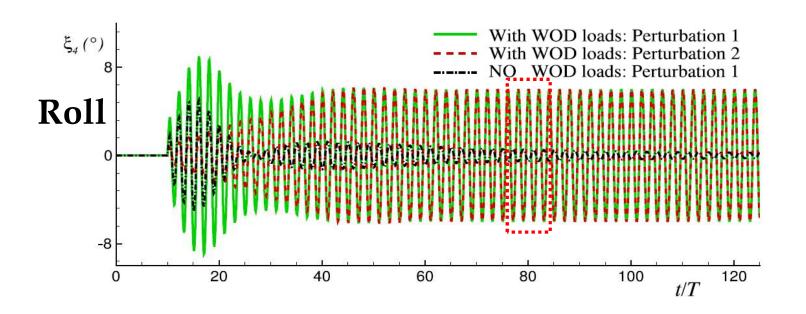


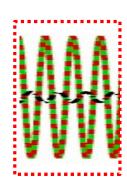
FPSO in head-sea regular waves





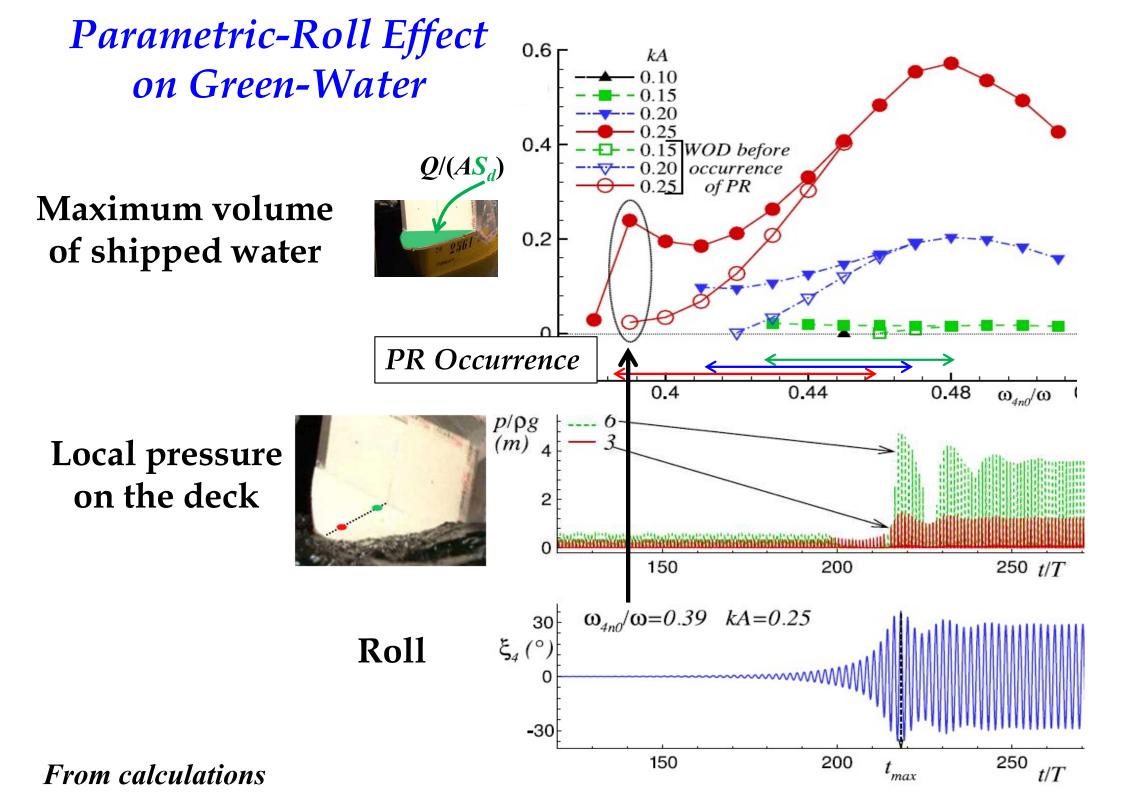
Green-water Effect on Parametric Roll





For PRs occurring both with and without WOD:

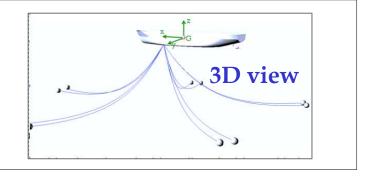
- ✓ WOD can increase or reduce the transient phase.
- ✓ WOD has a limited effect on the roll amplitude.



Green Water - Bilge Keels and Mooring lines

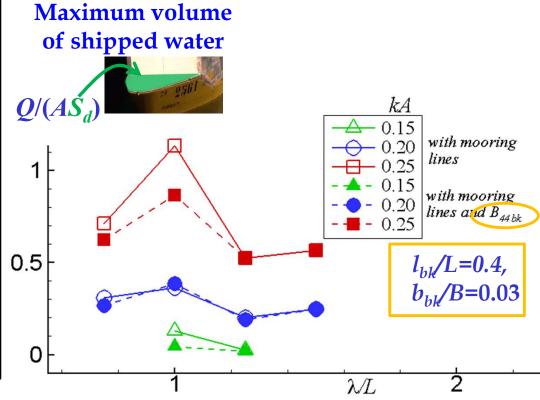
From systematic study including:

- Bilge-keel roll damping *B*_{44,bk}
- Mooring-line system



- ✓ Bilge-keel damping reduces roll and then the amount of WOD affected by roll.
- ✓ Mooring-line system leads to greater water on deck.

Without mooring-lines						
$rac{\lambda/L ightarrow}{\omega_{4n0}/\omega ightarrow}$	0.75	1.00	1.25	1.50	2.00	
$\omega_{4n0}/\omega \rightarrow$	0.402	0.464	0.519	0.568	0.656	
Method kA	Water On Deck (WOD)					
Exp. 0.10	NO	NO	NO	NO	NO	
No BK 0.10	NO	NO	NO	NO	NO	
With BK 0.10		NO				
Exp. 0.15	NO	NO	NI	NO	NO	
No BK 0.15	NO	0.017	0.012	NO	NO	
With BK 0.15		0.004				
Exp. 0.20	YES	YES	YES	YES	X	
No BK 0.20	0.125	0.178	0.134	0.017	X	
With BK 0.20	NO	0.177				
Exp. 0.25	YES	YES	YES	YES	X	
No BK 0.25	0.190	0.507	0.356	0.055	X	
With BK 0.25	0.036	5,41,845,41				



From calculations

Experiments vs numerics: Parametric roll & water on deck

β=175°

$\lambda/L ightarrow$	0.75	1.00	1.25	1.50	2.00	0.75	1.00	1.25	1.50	2.00
							20% H22 W		- 142 10000	10.28
Method kA	Parametric Roll				Water On Deck					
Exper. 0.10	NO	YES	NO	NO	NO	NO	NO	NO	NO	NO
Num 0.10	NO	YES	NO	NO	NO	NO	NO	NO	NO	NO
Exper. 0.15	NO	YES	NO	NO	NO	NO	small	small	small	NO
Num 0.15	NO	YES	NO	NO	NO	NO	YES	YES	small	NO
Exper. 0.20	YES	YES	NO	YES	X	due to PR	YES	YES	YES	X
Num 0.20	YES	YES	NO	NO	X	due to PR	YES	YES	YES	X
Exper. 0.25	YES	NO	NOYES	YES	X	YES	YES	YES	YES	X
Num 0.25	YES	NO	NO	NO	X	YES	YES	YES	YES	X

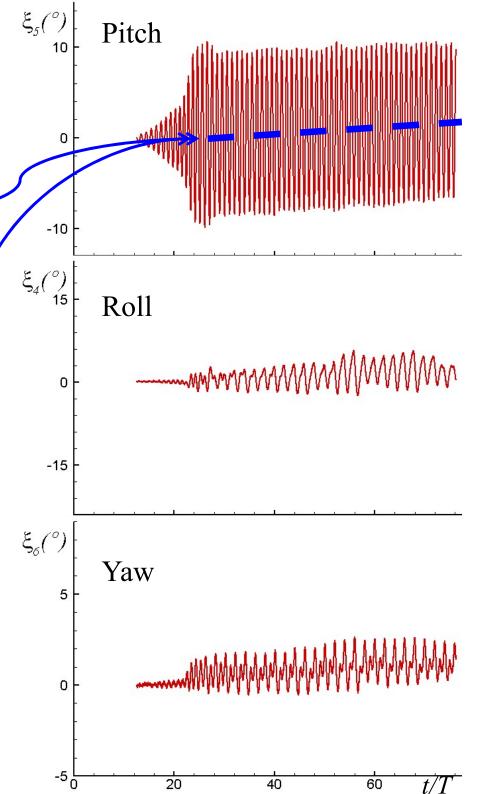
Run 44

Run 46

Experiments: Run 44

Front view





Side view

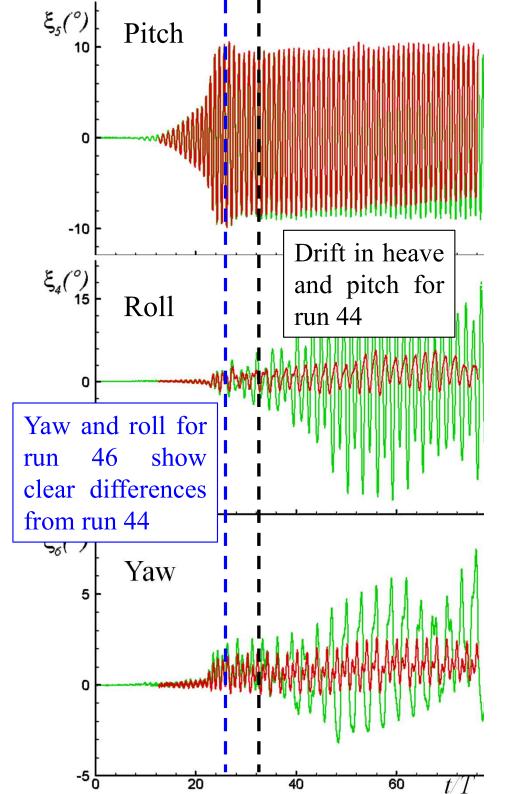
Experiments: Run 46

Front view

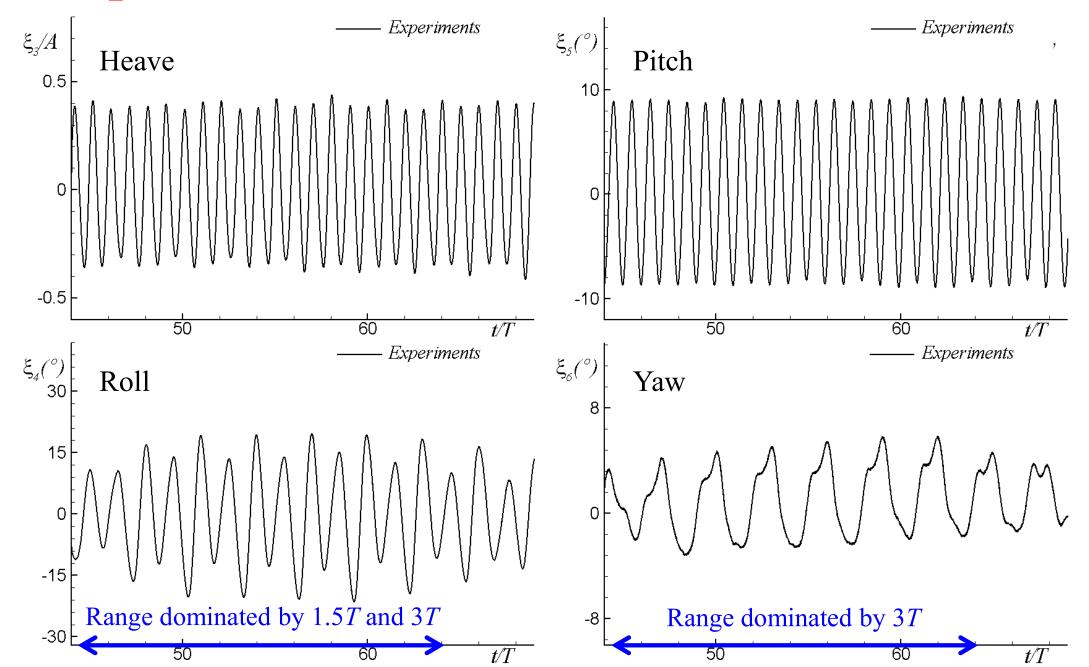


Side view

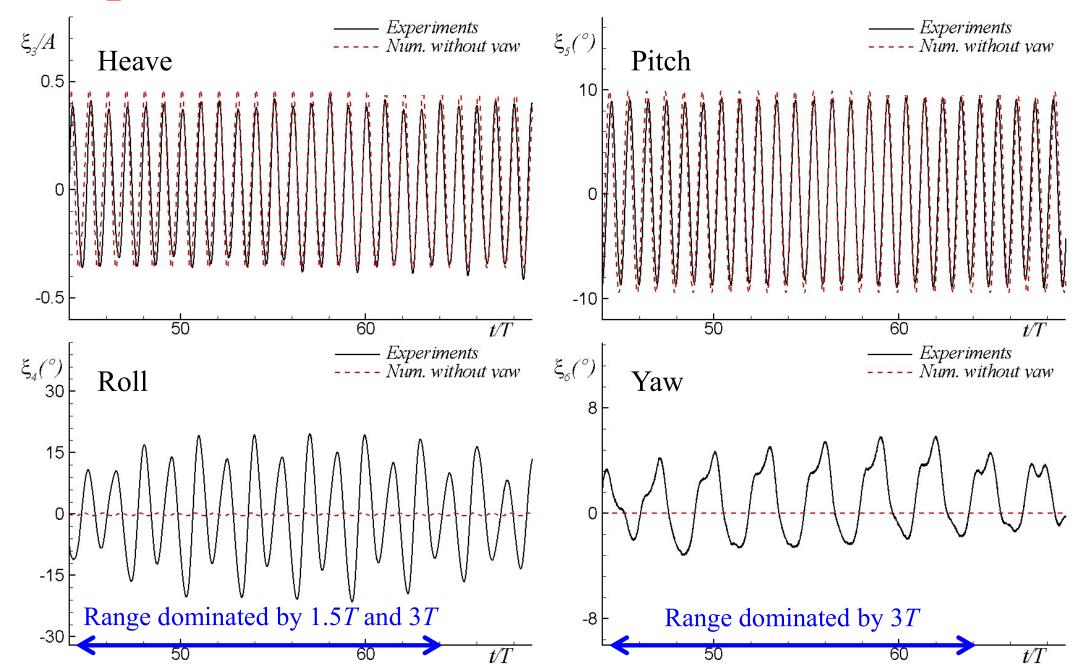




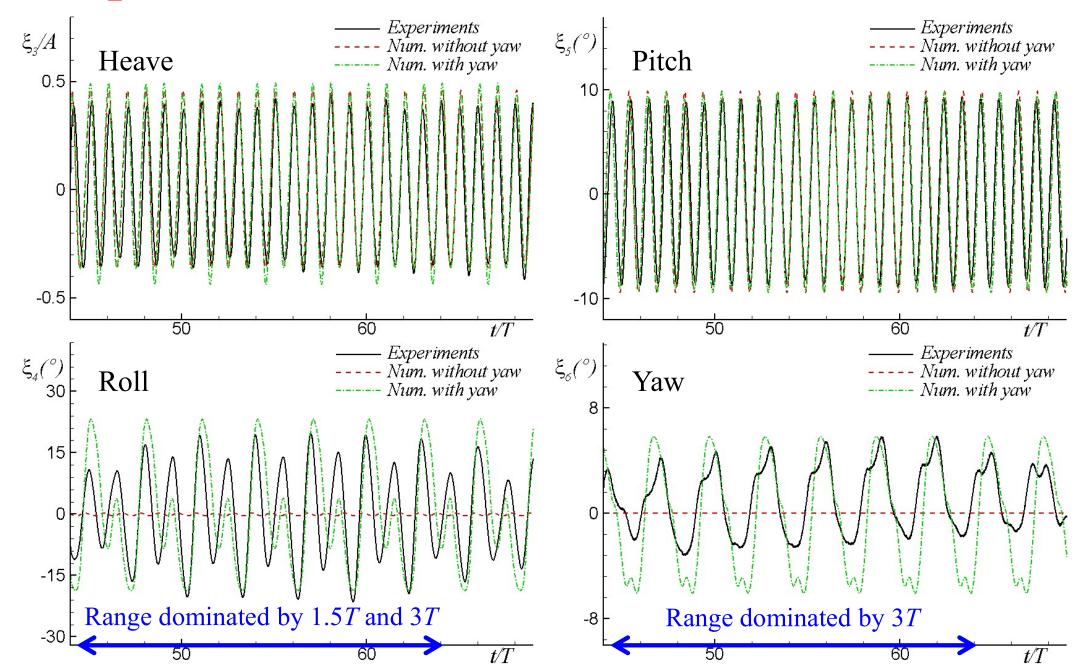
Assessment of roll-yaw coupling effects: Experiments (Run 46) vs numerics - Motions



Assessment of roll-yaw coupling effects: Experiments (Run 46) vs numerics - Motions

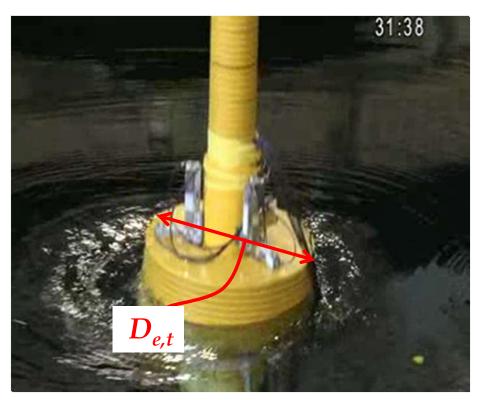


Assessment of roll-yaw coupling effects: Experiments (Run 46) vs numerics - Motions



Green Water and Dynamic Response: a Combined Wind and Wave Energy Converter Concept in Survival Conditions

Model tests



$$6 < MD_{e,t} < 18$$

 $H = 2A = 9m$ (full scale)
 $→ kA ∈ [0.08, 0.22]$

✓ 'Nonlinear' FK+ hydrostatic loads within longwave approximation do not capture the physics.

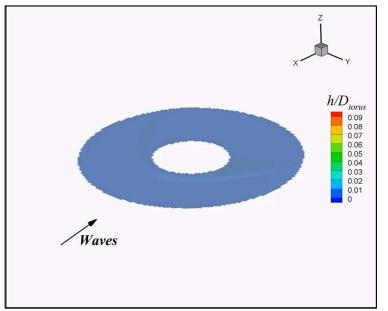
Green Water and Dynamic Response: a Combined Wind and Wave Energy Converter Concept in Survival Conditions

Numerical DD2 results

Model tests

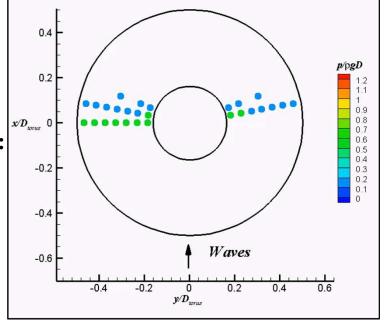


3D view: Green Water



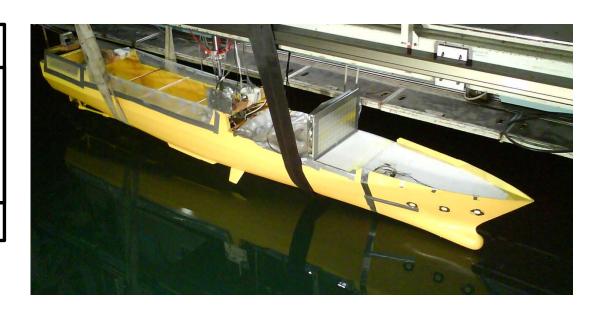
✓ For this case, the water on deck influences the platform motions.

Bottom view: Slamming

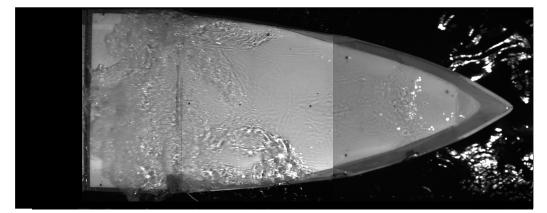


Green Water and Forward Speed: a Patrol Ship

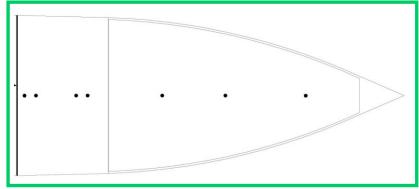
	Full scale		
Length (L)	80.0 m		
$\operatorname{Breadth}(B)$	$12.2 \mathrm{\ m}$		
Draft (D)	$3.24 \mathrm{\ m}$		
Freeboard (f)	0.58 m		
<i>Scale 1:20</i>			



Water on deck



Green-water loads



Water-On-Deck Occurrence: Fr = 0

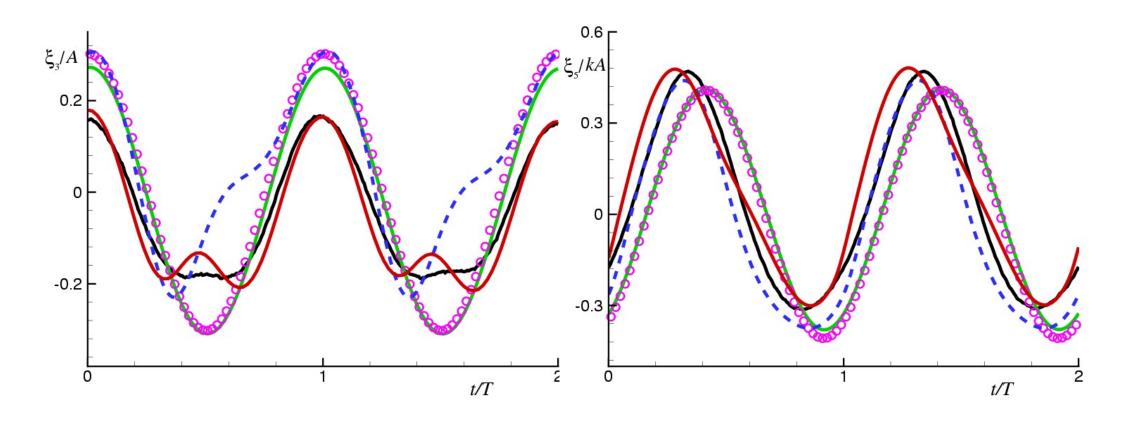
Regular head-sea waves

Water on deck and Body Motions

 $kA \cong 0.25, \ \lambda / L = 1, Fr = 0$

Heave motion

Pitch motion



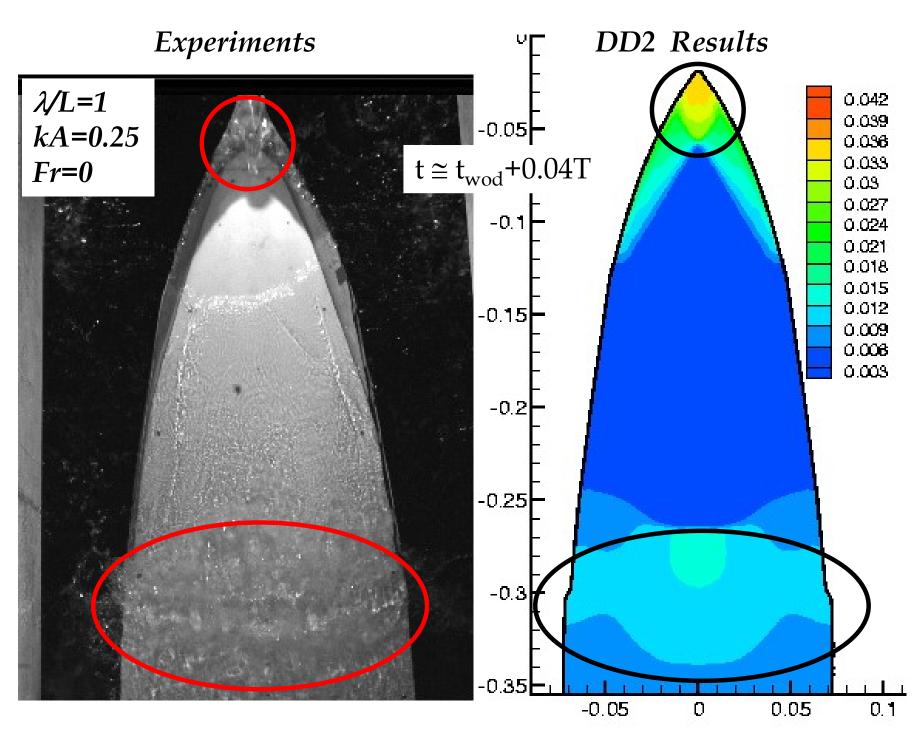
Experiments

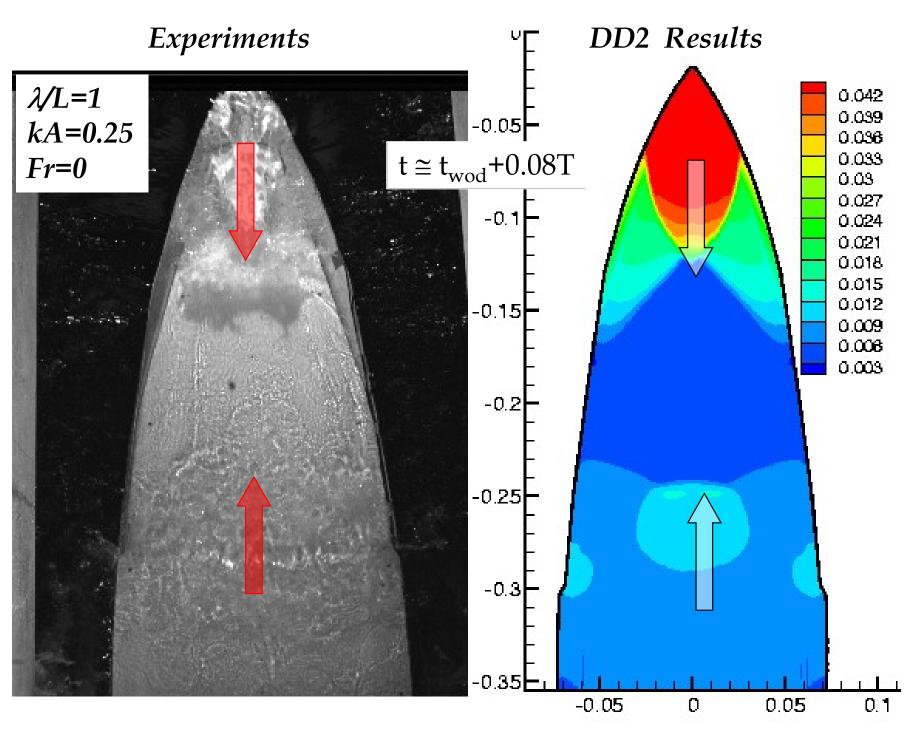
DD2: Linear without wod

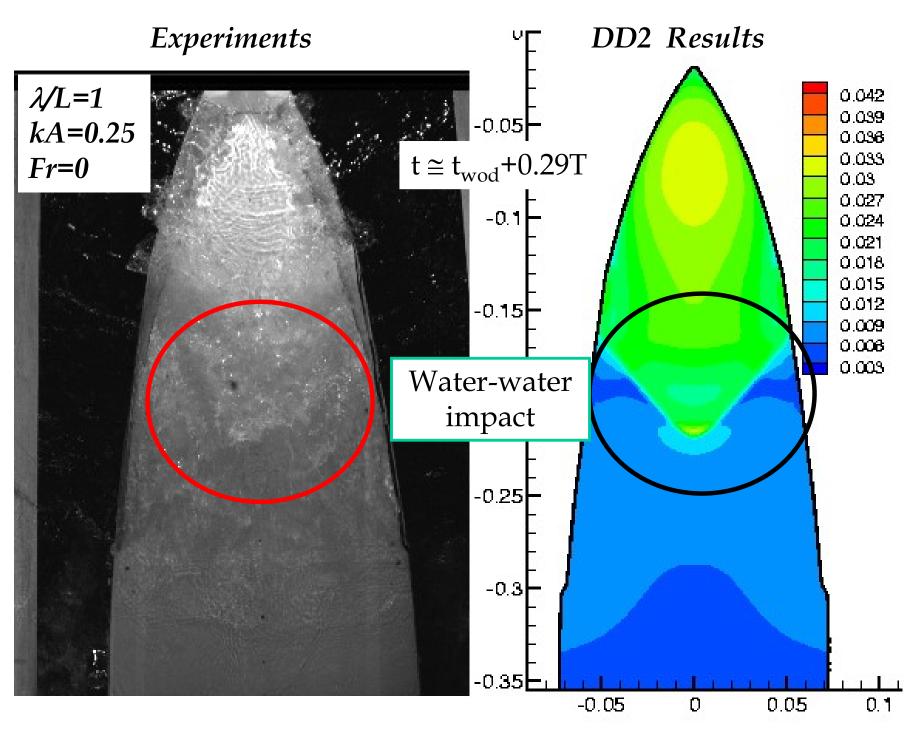
DD2: Linear with wod

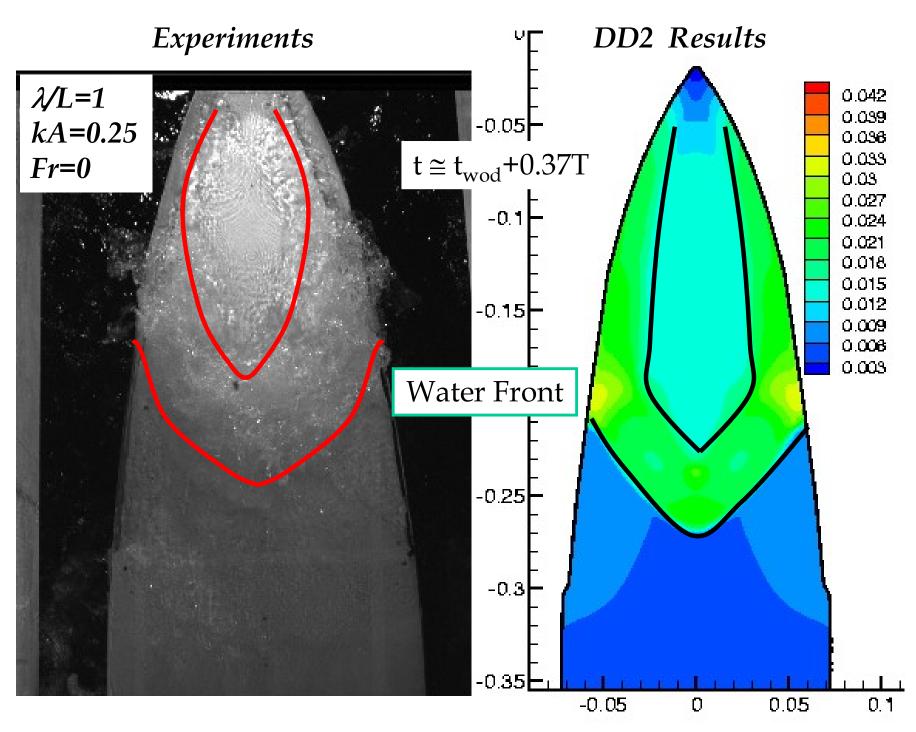
DD2: Wnl without wod

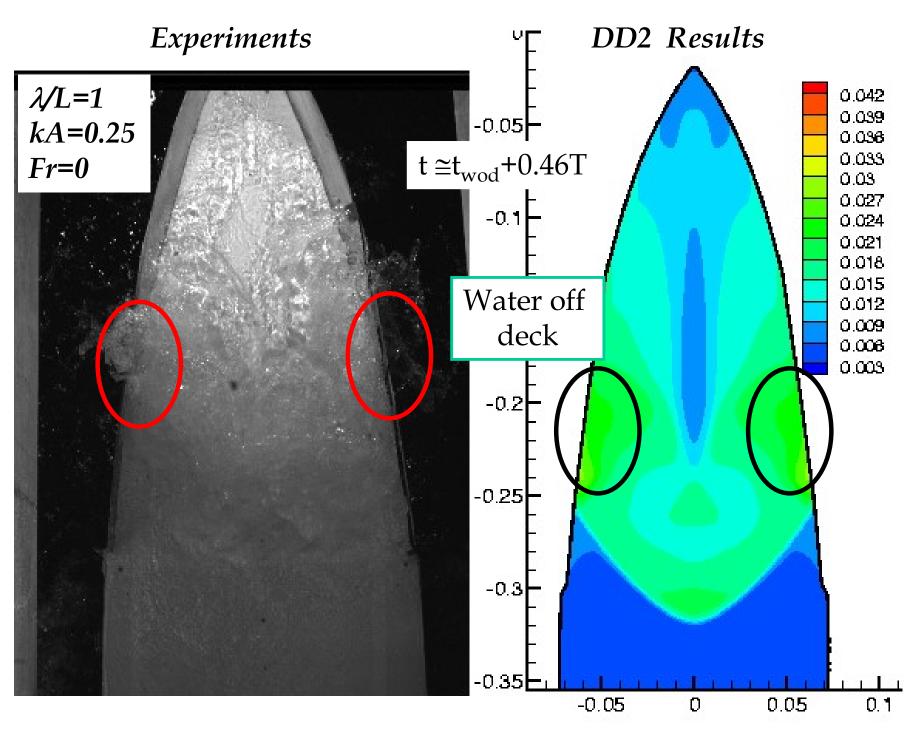
DD2: Wnl with wod

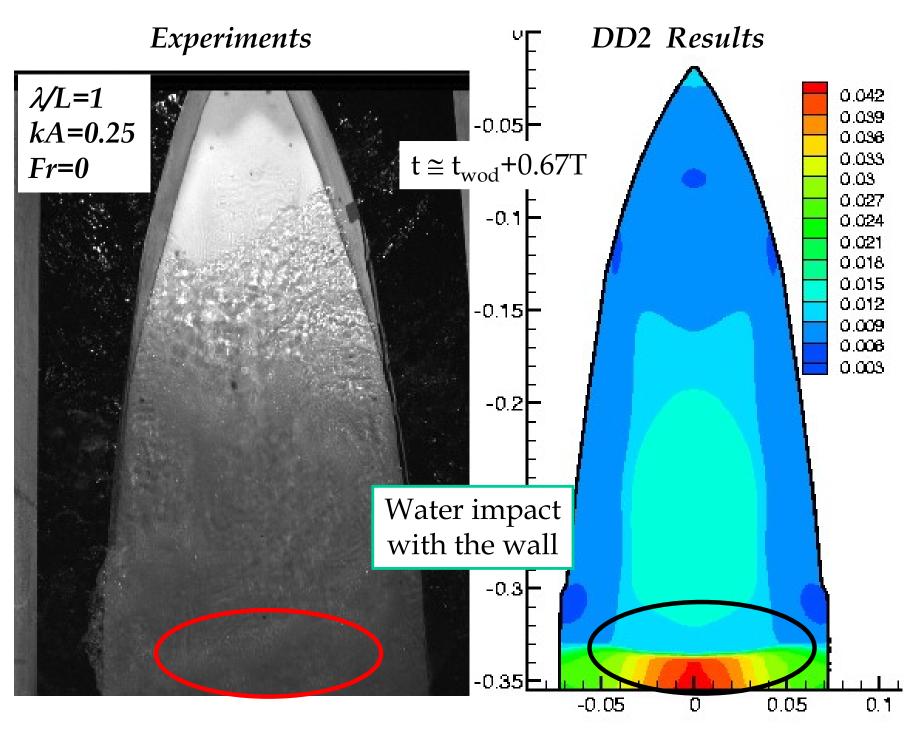






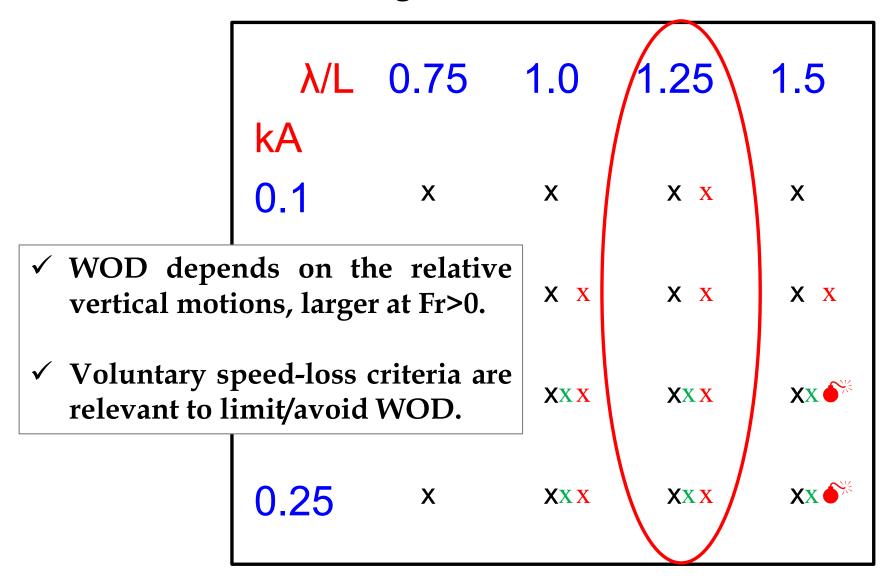




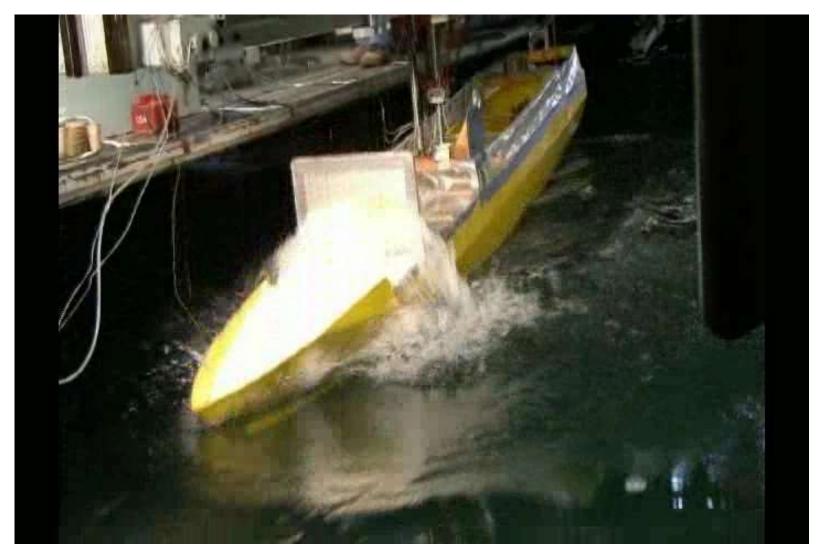


Water-On-Deck: Fr = 0 versus Fr = 0.189

Regular head-sea waves



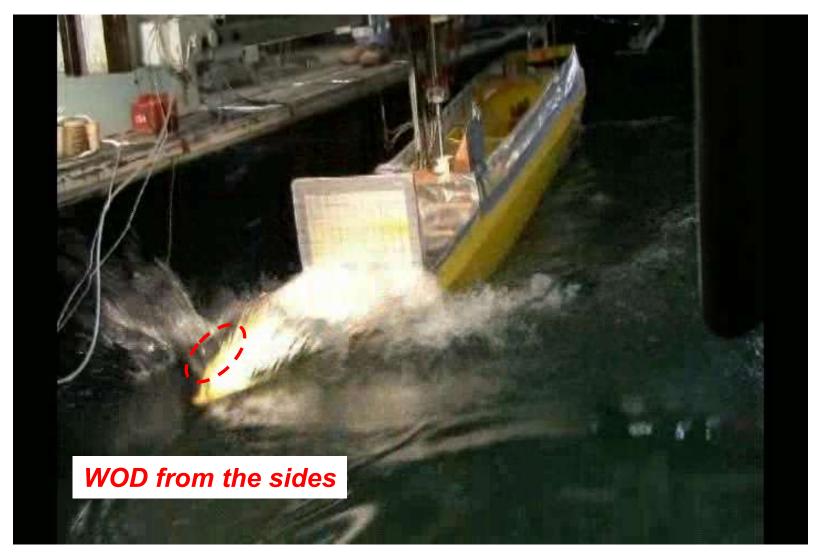
From experiments

















Flow on the Deck ($\lambda/L=1.25$)

kA=0.15 Fr=0

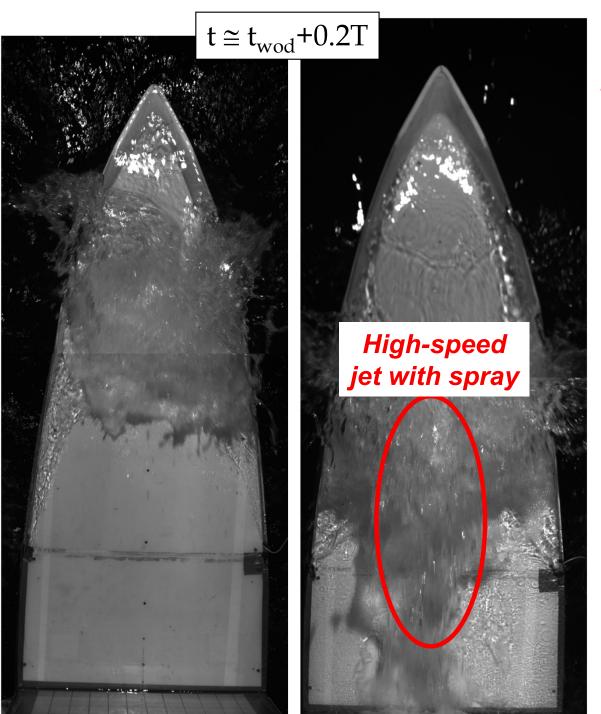


kA = 0.25 Fr = 0



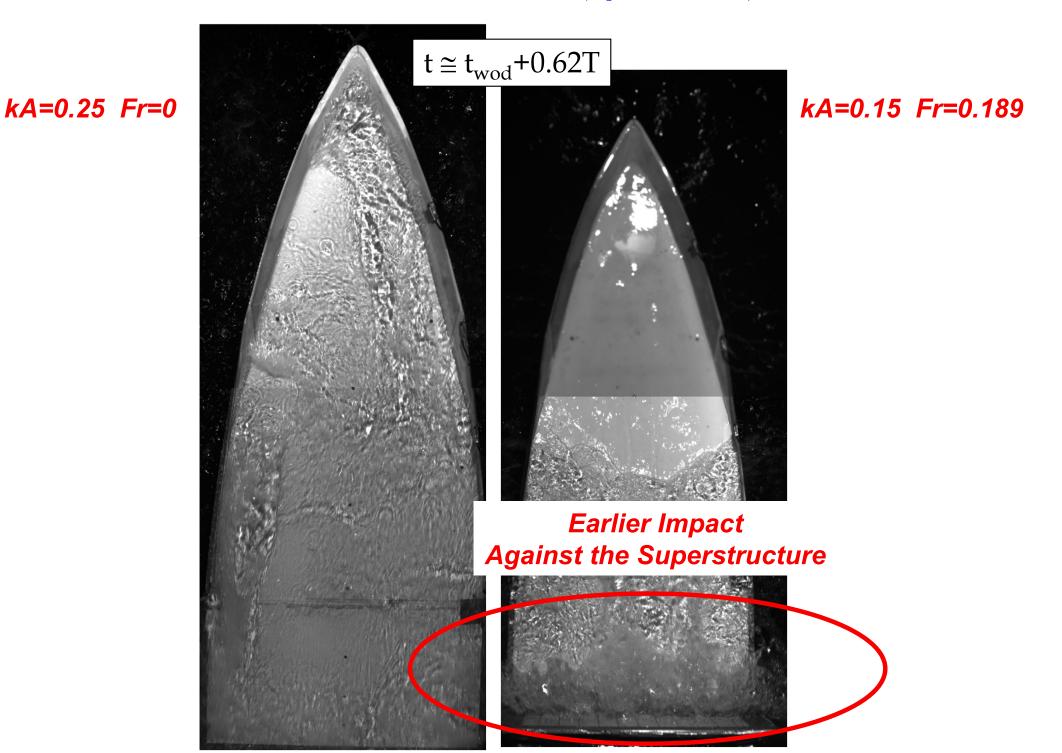
Flow on the Deck ($\lambda/L=1.25$)

kA=0.25 Fr=0

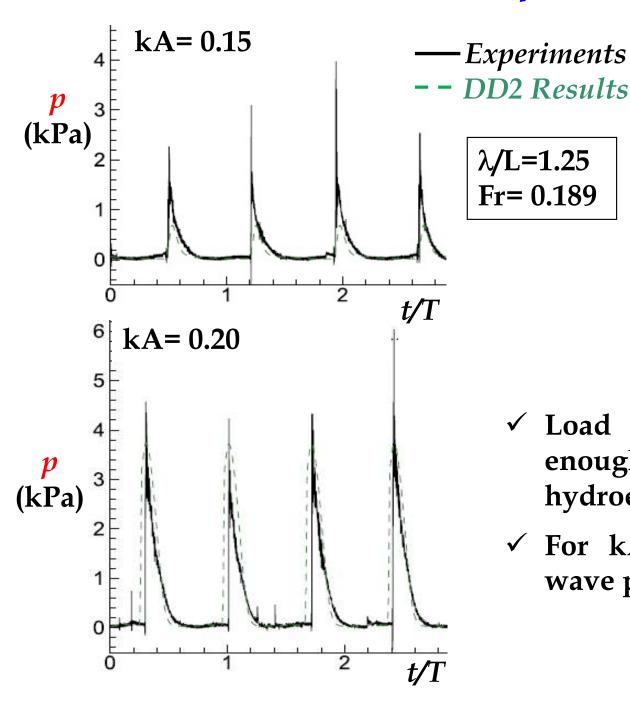


kA=0.15 Fr=0.189

Flow on the Deck ($\lambda/L=1.25$)



Green Water: Local pressure on front deck



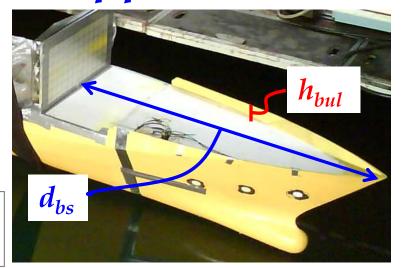


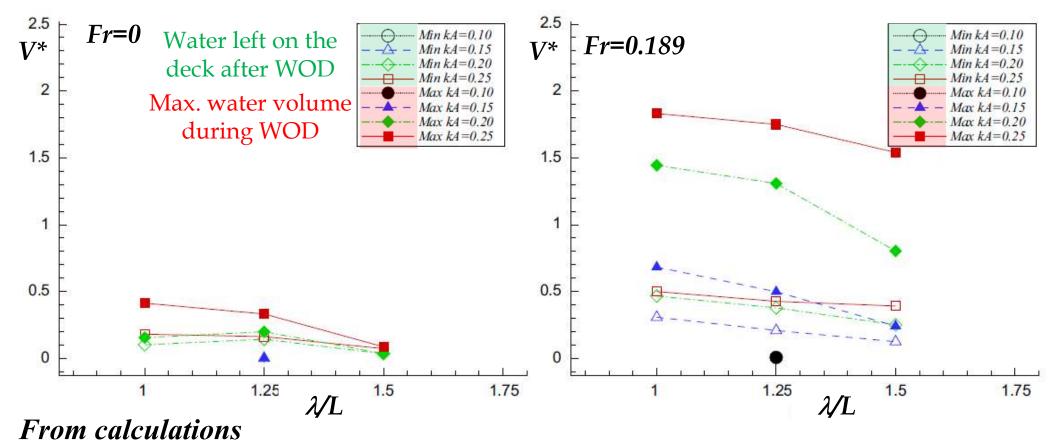
- ✓ Load 'duration' must be small enough for triggering local hydroelasticity.
- ✓ For kA=0.2, it is ~10-20% of the wave period, so relatively large.

Water-on-deck: Volume of shipped water

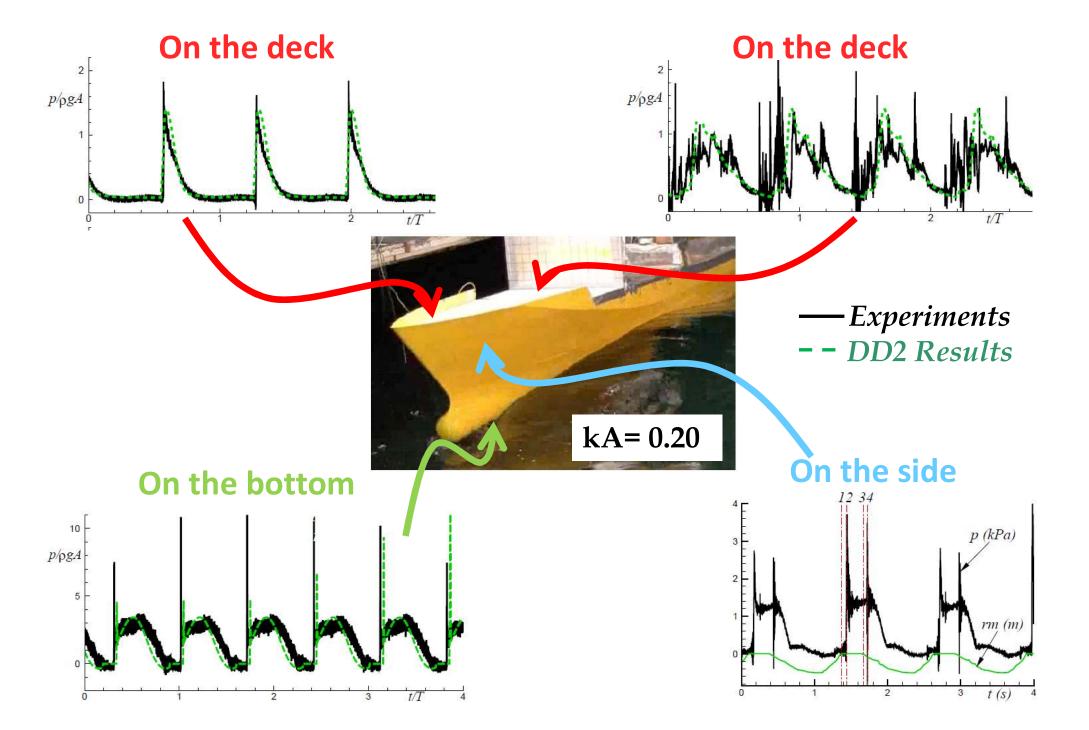
- ✓ The water left on the deck could endanger in principle the transverse stability.
- ✓ It is larger at Fr=0.189 but, as roll was restrained, this aspect was not examined.

 $V^*=V/(h_{bul} d_{bs} B)$ h_{bul} = height of bulwark d_{bs} =front bow-superstructure distance B=ship breath





Water-on-deck & slamming: Local pressure

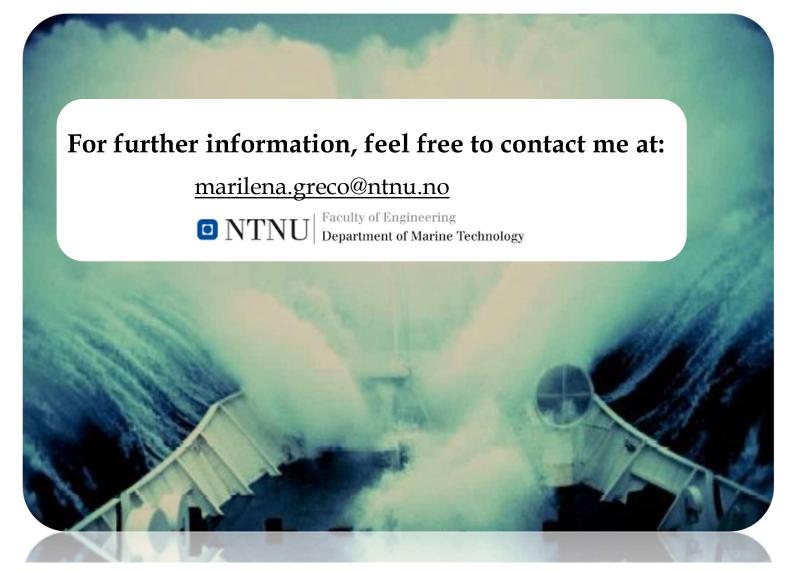


Green Water - Few Key Points

Among the Scenarios, PDB type seems the most common. For most of the types, both wave and body parameters matter; but for large-scale PW the body has less influence.

- Green-Water Loads can be dangerous for ships or platforms; their structural consequences may be analyzed using either a quasi-static or a hydroelastic approach, depending on the scenario.
- ☐ Transient and Dynamic Effects can matter for the loads and structural response even in long waves.

Thank You!



Konstruksjonsdagen 2025