



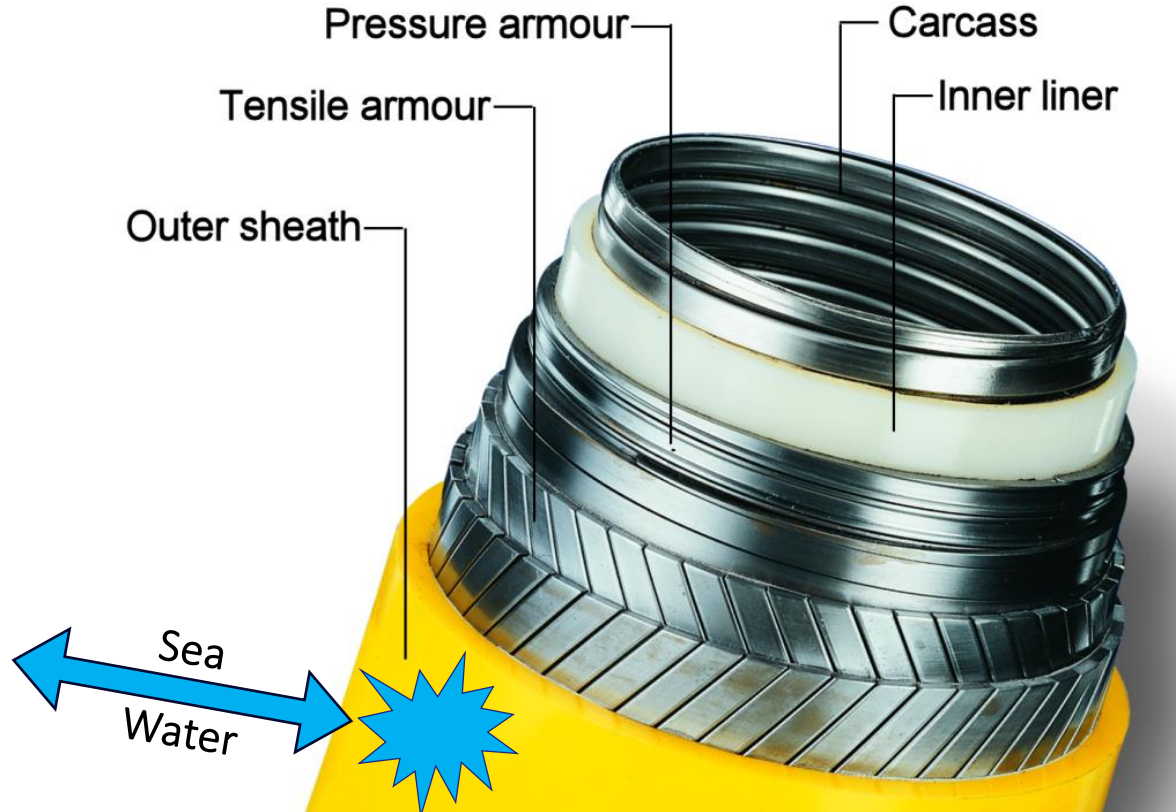
16.11.2025

Fagdag om fleksible rør, integritetsstyring og aldring,
HAVTIL Stavanger 26 th November 2025

Corrosion of armour wire steel in the annulus of flexible pipes - an overview of mechanisms

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Corrosion modes / mechanisms



Confined environment

- $V/S < 0.1 \text{ ml/cm}^2$

Diffusion:

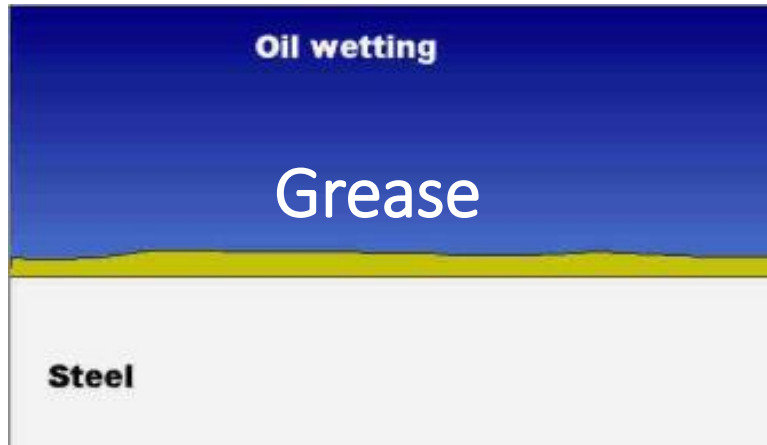
- H_2O (high RH%- liquid)
- CO_2
- H_2S
- CH_4 +++

Air (O_2) through vent port

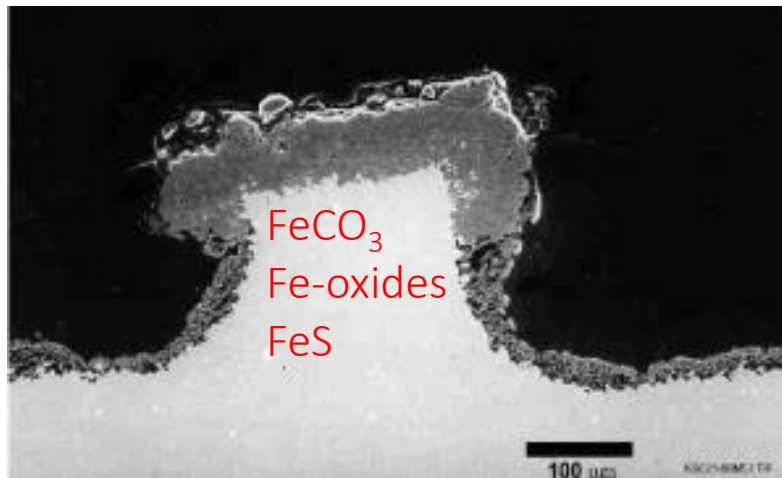
Damaged outer sheath:

- air (20 % O_2)
- sea water (0-10 ppmw)

Carbon steel exposed to water + CO₂/H₂S/O₂ in the annulus corrodes $\gg 0.01$ mm/y unless it achieves a protective layer on the surface



CP?



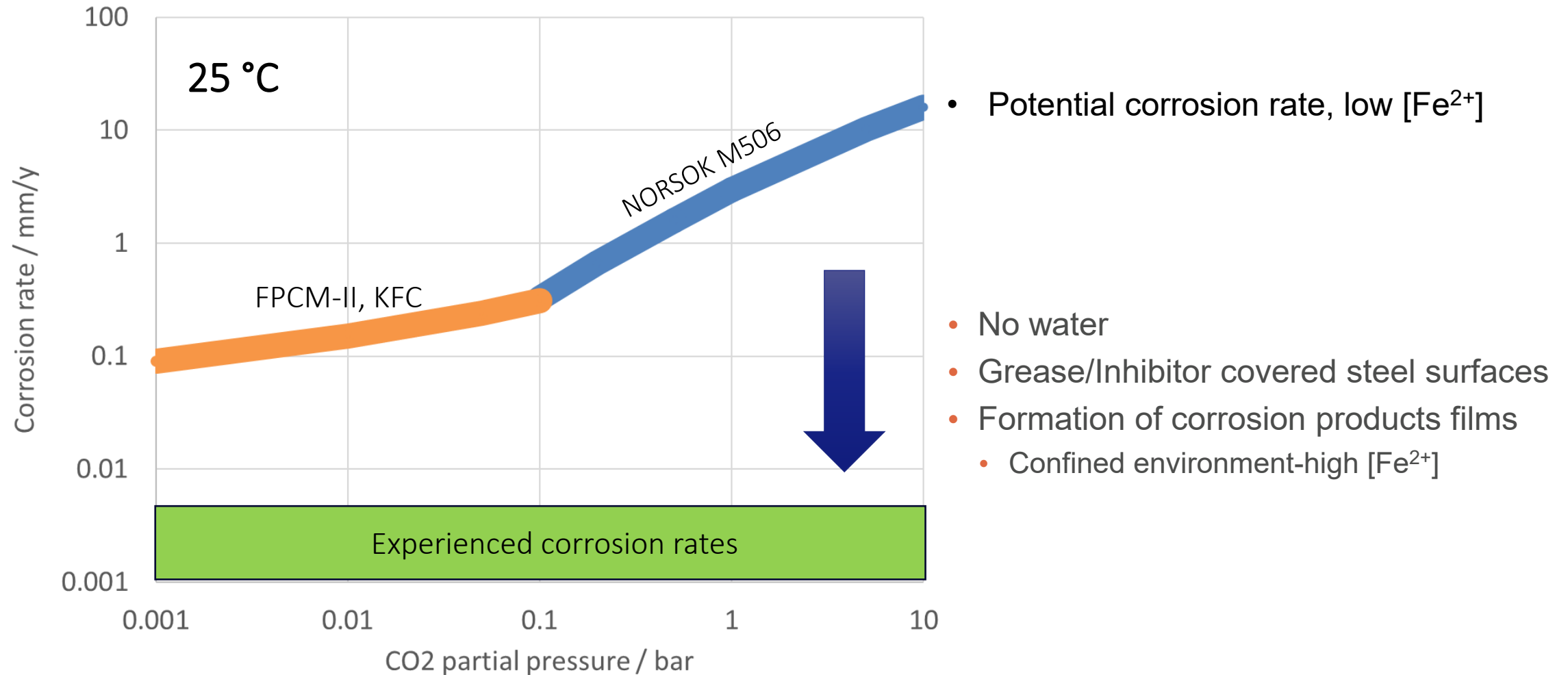
Local corrosion rates for water wet wire surfaces

| Temp °C ↓ | $pCO_2 \rightarrow$ | <0.01 | 0.01-0.1 | 0.1-0.5 | >0.5 | Air (<i>amb</i>) |
|-----------|-----------------------|---------------------|----------|---------|---------|--------------------|
| | | Corrosion rate mm/y | | | | |
| < 30 | High Fe ²⁺ | < 0.01 | < 0.01 | < 0.01 | < 0.01 | <0.15 |
| | Low Fe ²⁺ | < 0.15 | < 0.4 | < 1 | > 1 | |
| | Post repair | < 0.05? | < 0.05? | < 0.05? | < 0.05? | |
| 30-50 | High Fe ²⁺ | < 0.01 | < 0.01 | < 0.01 | < 0.01 | <0.20 |
| | Low Fe ²⁺ | <0.25 | <0.8 | <1.5 | >1.5 | |
| | Post repair | < 0.05? | < 0.05? | < 0.05? | < 0.05? | |
| 50-70 | High Fe ²⁺ | < 0.01 | < 0.01 | < 0.01 | < 0.01 | <0.30 |
| | Low Fe ²⁺ | <0.25 | <1 | <2 | >2 | |
| | Post repair | < 0.05? | < 0.05? | < 0.05? | < 0.05? | |
| >70 | High Fe ²⁺ | < 0.01 | < 0.01 | < 0.01 | < 0.01 | <0.30 |
| | Low Fe ²⁺ | <0.25 | <1.2 | <2.5 | >2.5 | |
| | Post repair | < 0.05? | < 0.05? | < 0.05? | < 0.05? | |

- **Green:** Good experimental data which is supported by field observation/experience.
- **Yellow:** Extrapolated data from lab and field.
- **Pink:** Not much data, need to be addressed.

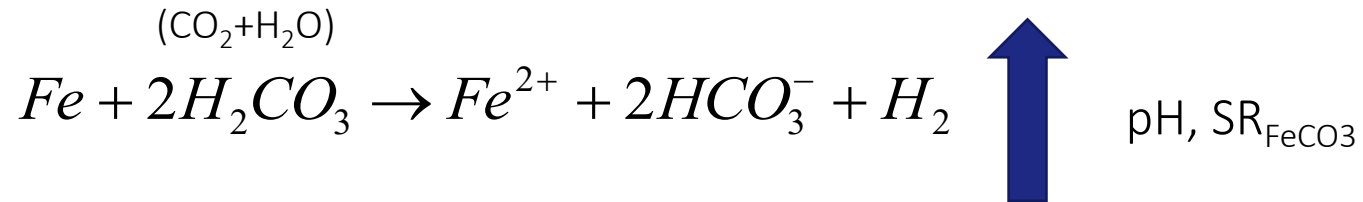
Normal situation, no outer damage, condensed water

Potential corrosion rate vs actual corrosion rate

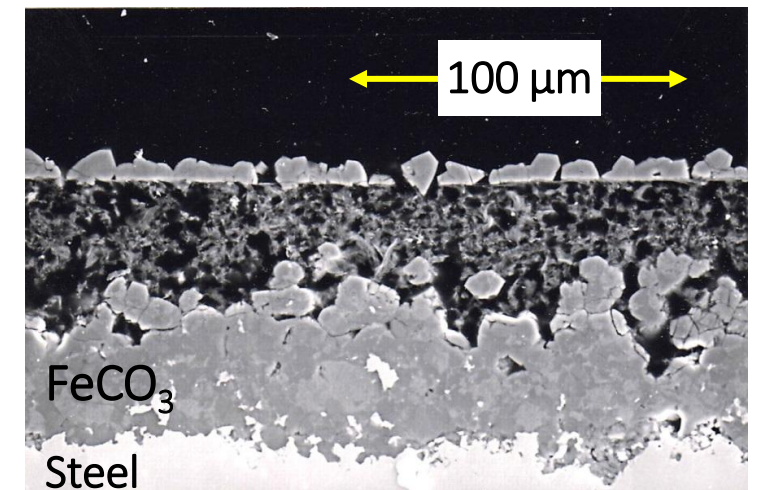
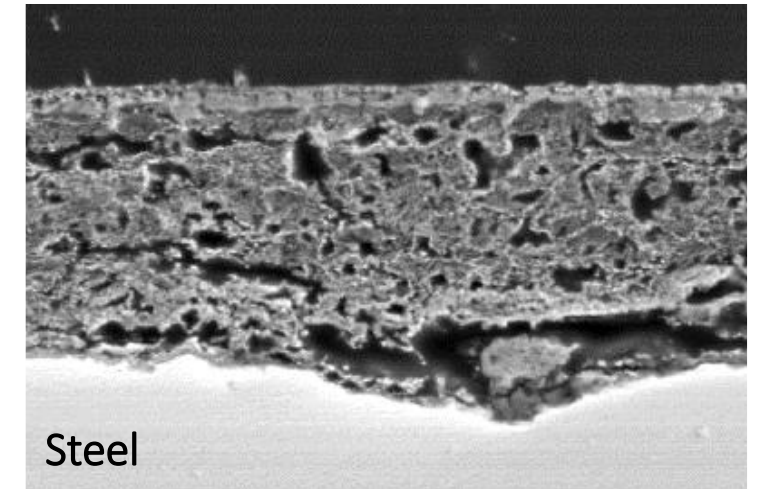
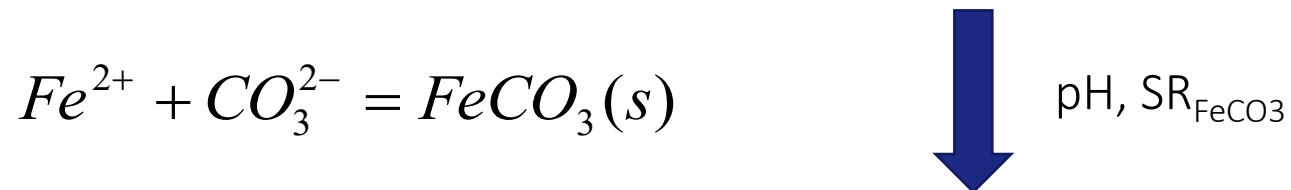


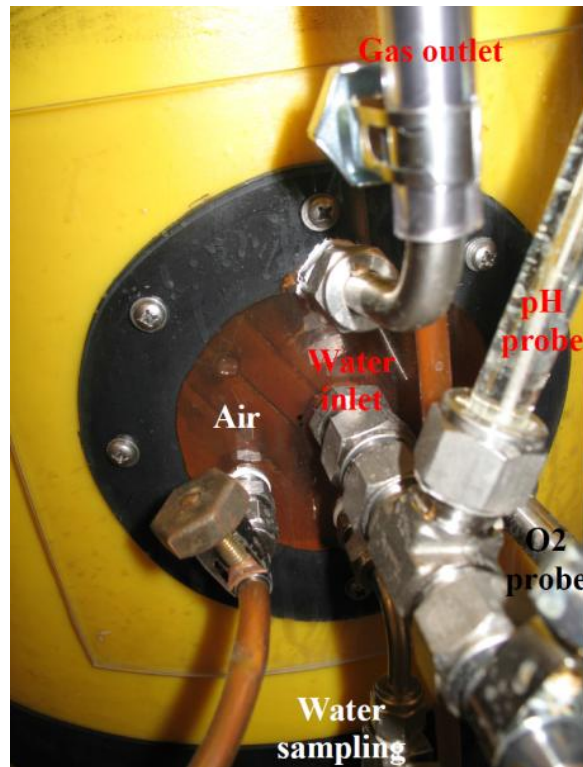
Normal situation, no outer damage, condensed water

Protective film formation dependent on pH, SR_{FeCO_3} and concentration of dissolved corrosion product

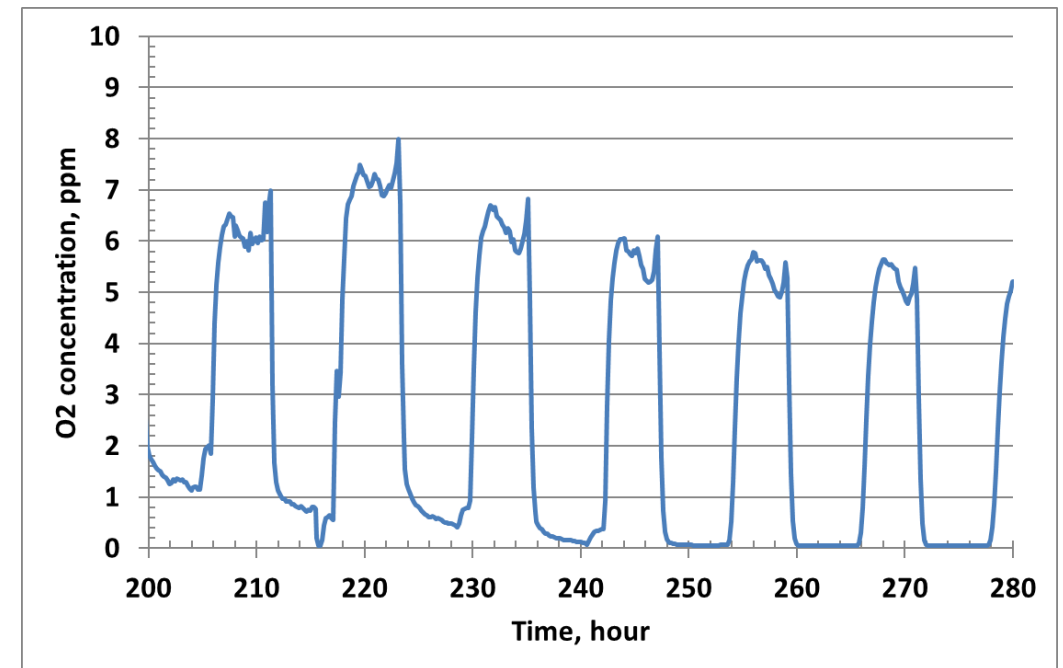
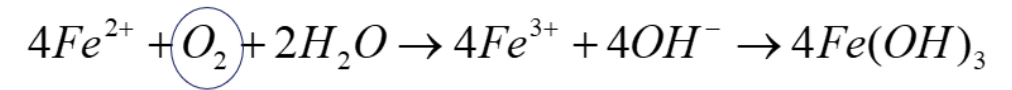
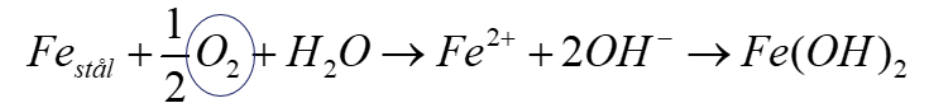


$$SR_{FeCO_3} = \frac{C_{Fe^{2+}} \cdot C_{CO_3^{2-}}}{K_{sp}} > 1 \quad \rightarrow \quad pH, SR_{FeCO_3} = 100-1000$$





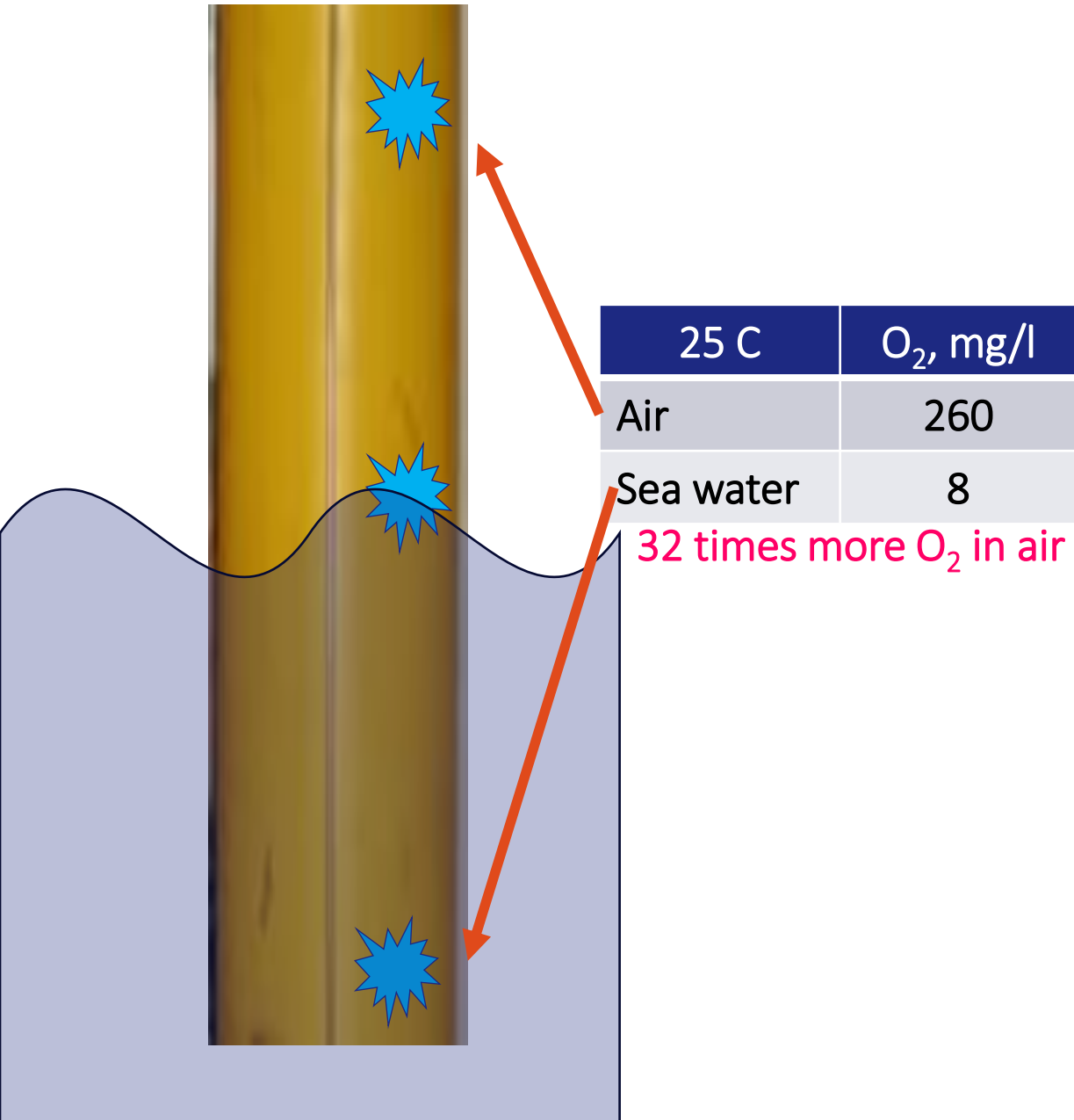
O₂ ingress- damaged outer sheath



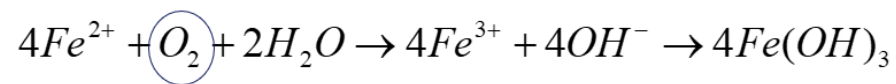
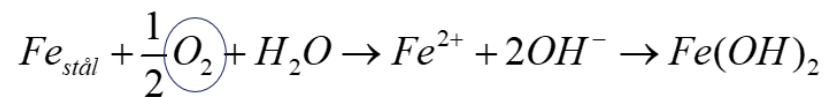
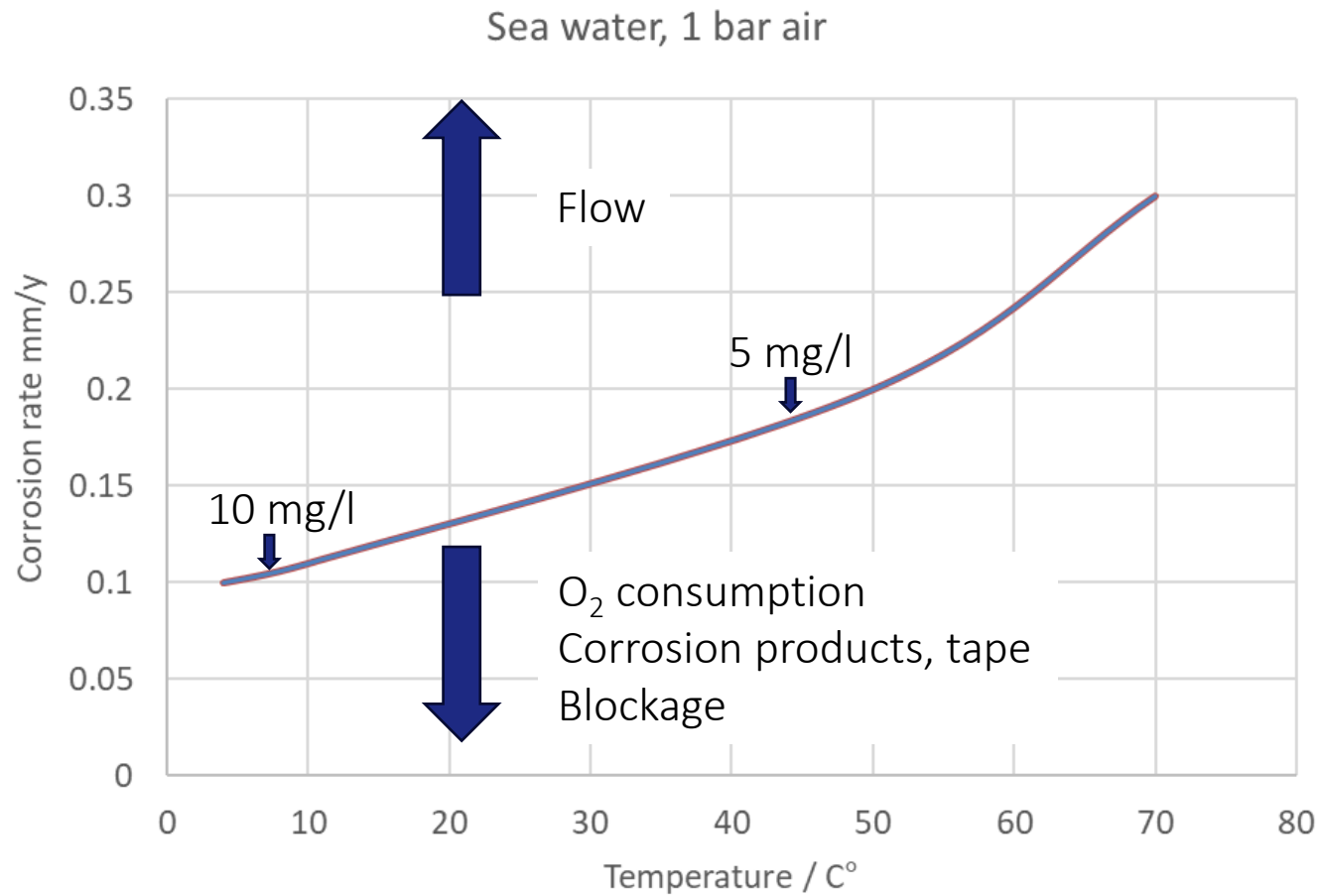
Corroded steel \propto water volume $\times [\Delta O_2]$

O_2 ingress

air/water pumping through vent port and damaged outer sheath



- Atmospheric pressure variation
- Tide water
- Waves
- Venting (pressure drop)
- Temperature variation
 - Shut down
- Open vent
 - Pressure variation vs dead volume vs permeation

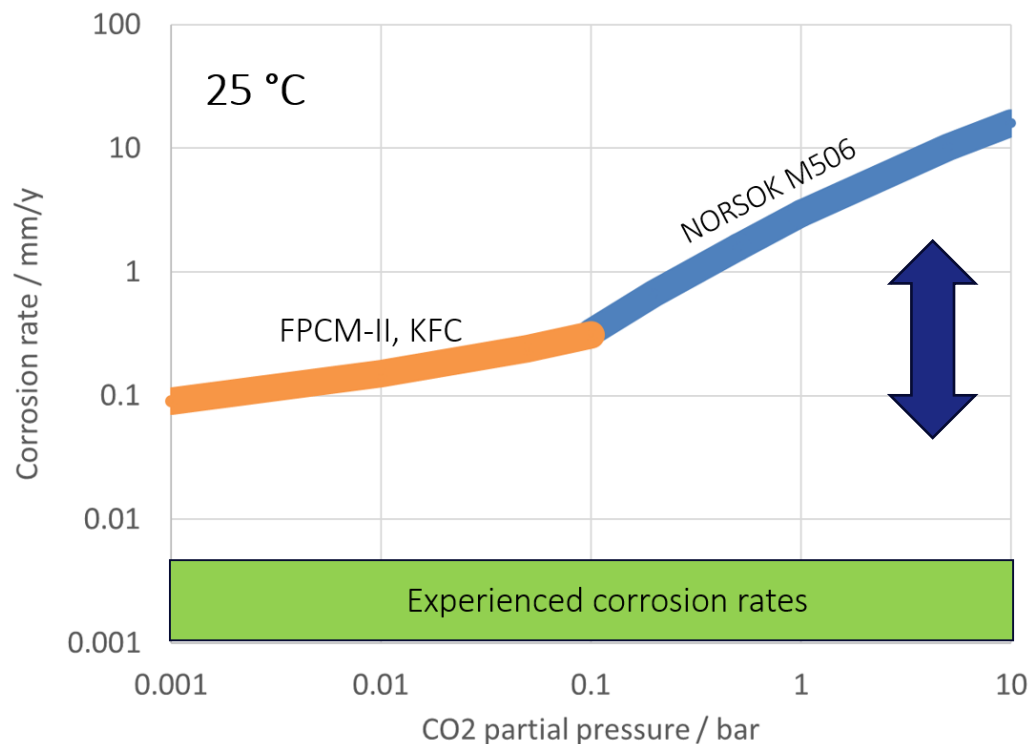


armour wire

armour wire

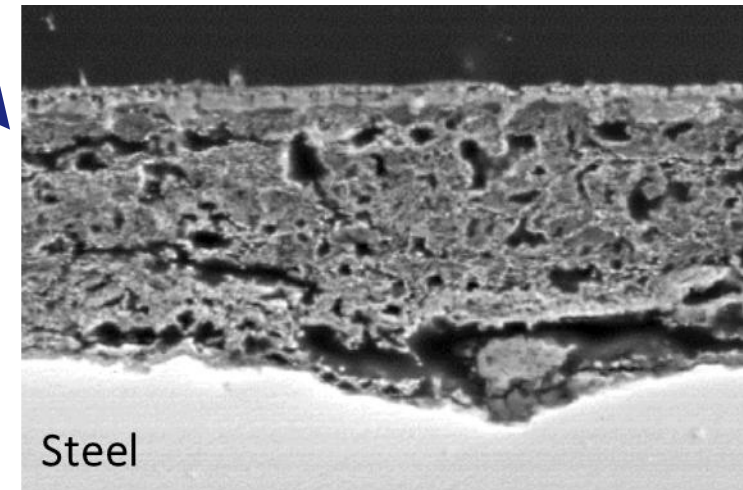
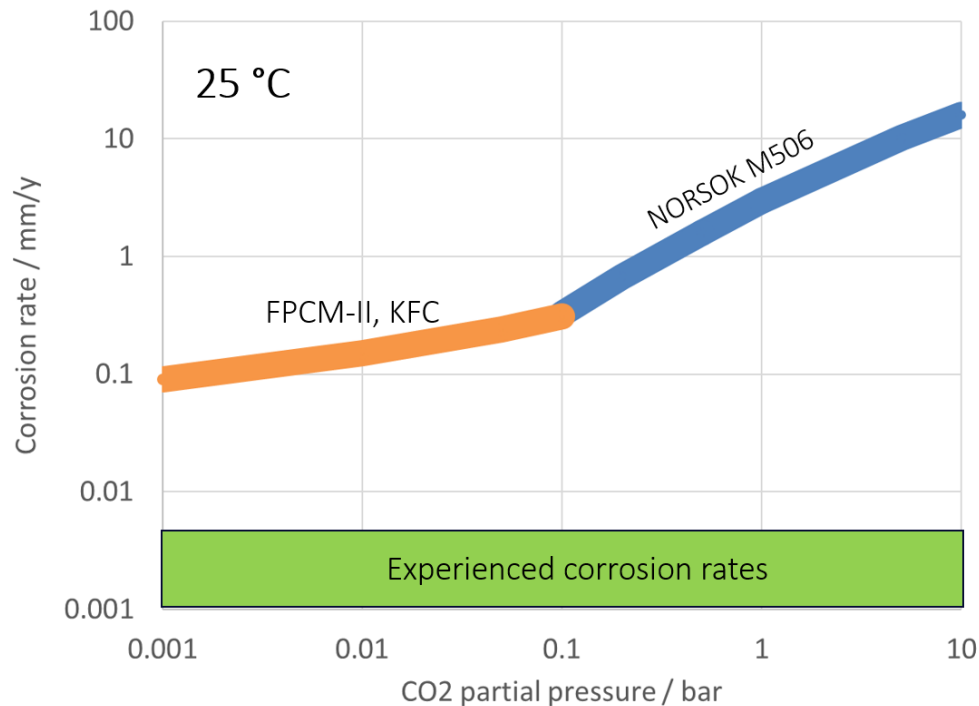
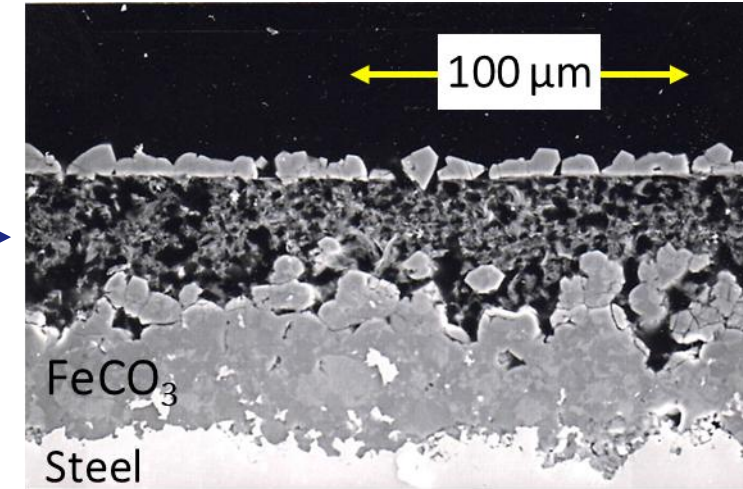
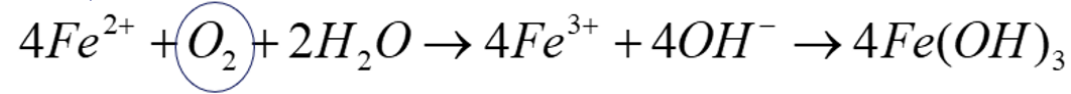
Low $[\text{Fe}^{2+}]$ combined with low CO_2 (hungry water)

| Temp °C ↓ | $p\text{CO}_2 \rightarrow$ | <0.01 | 0.01-0.1 | 0.1-0.5 | >0.5 | Air (<i>amb</i>) |
|-----------|----------------------------|---------------------|----------|---------|---------|--------------------|
| | | Corrosion rate mm/y | | | | |
| < 30 | High Fe^{2+} | < 0.01 | < 0.01 | < 0.01 | < 0.01 | <0.15 |
| | Low Fe^{2+} | < 0.15 | < 0.4 | < 1 | > 1 | |
| | Post repair | < 0.05? | < 0.05? | < 0.05? | < 0.05? | |



1. Backflow of condensed water from the vent system
2. Consumption of Fe^{2+}

CO₂ combined with O₂

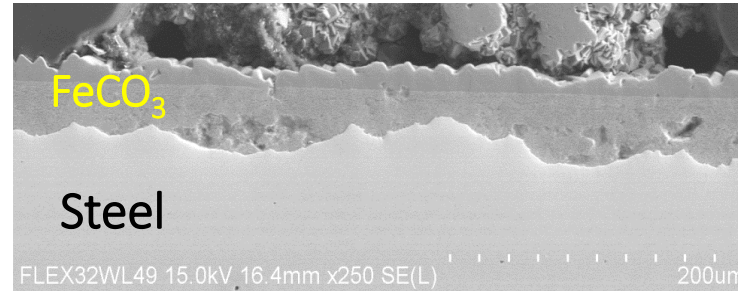


Post repair ?

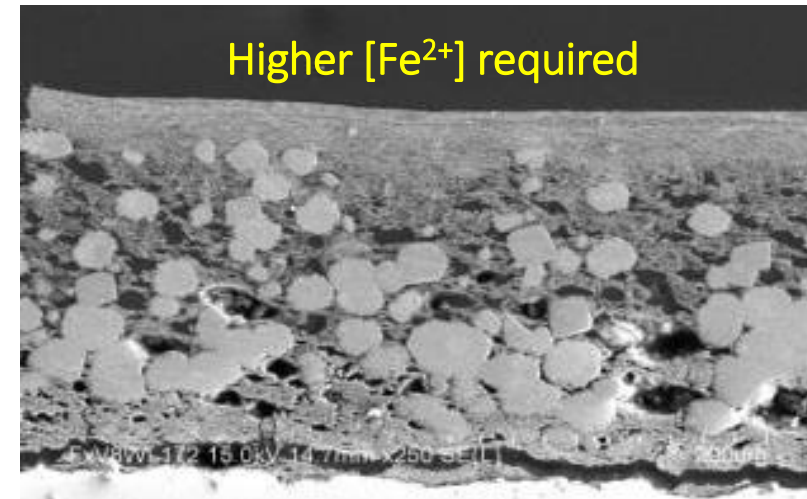
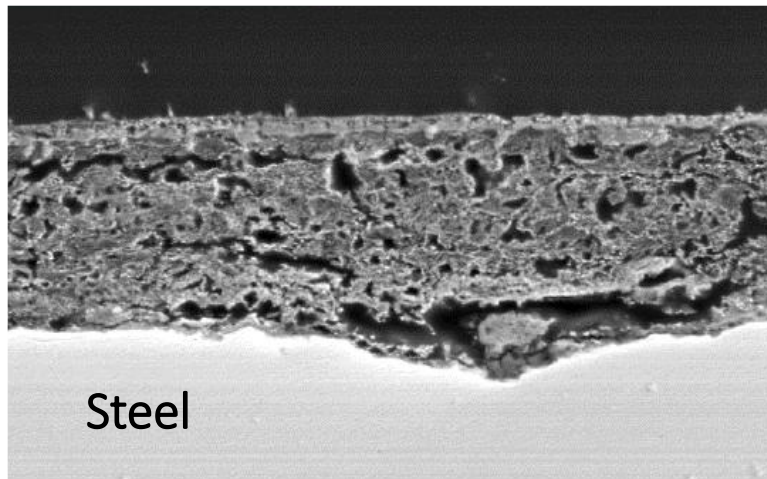
| Temp °C ↓ | $pCO_2 \rightarrow$ | <0.01 | 0.01-0.1 | 0.1-0.5 | >0.5 | Air (<u>amb</u>) |
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| | | Corrosion rate mm/y | | | | |
| < 30 | High Fe^{2+} | < 0.01 | < 0.01 | < 0.01 | < 0.01 | <0.15 |
| | Low Fe^{2+} | < 0.15 | < 0.4 | < 1 | > 1 | |
| | Post repair | < 0.05? | < 0.05? | < 0.05? | < 0.05? | |

The required $[\text{Fe}^{2+}]$ to achieve and
maintain protection is «history» dependent

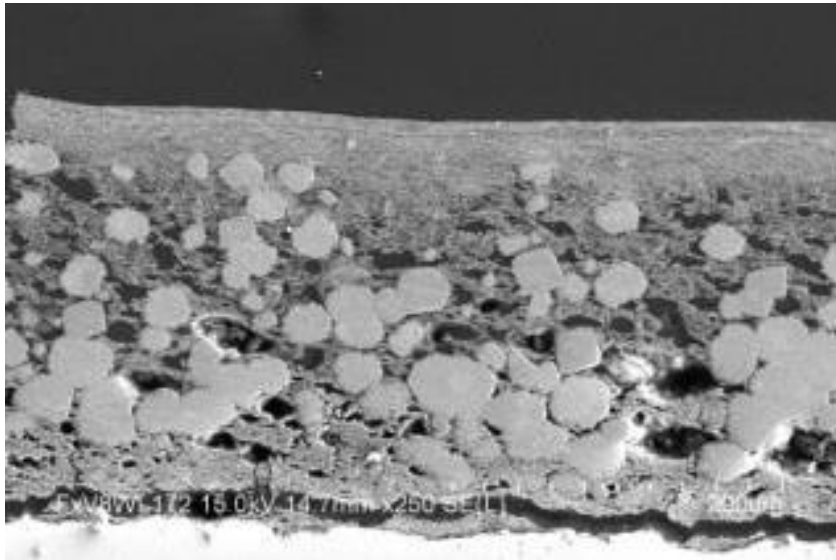
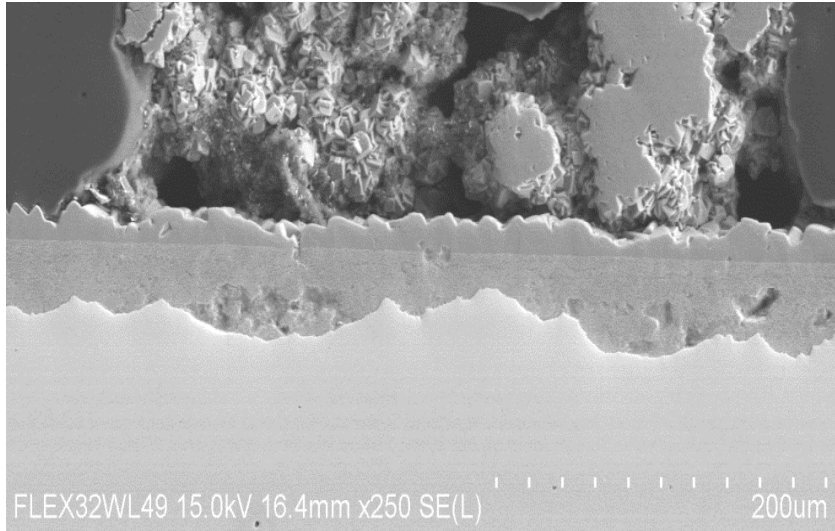
CO_2 - exposure



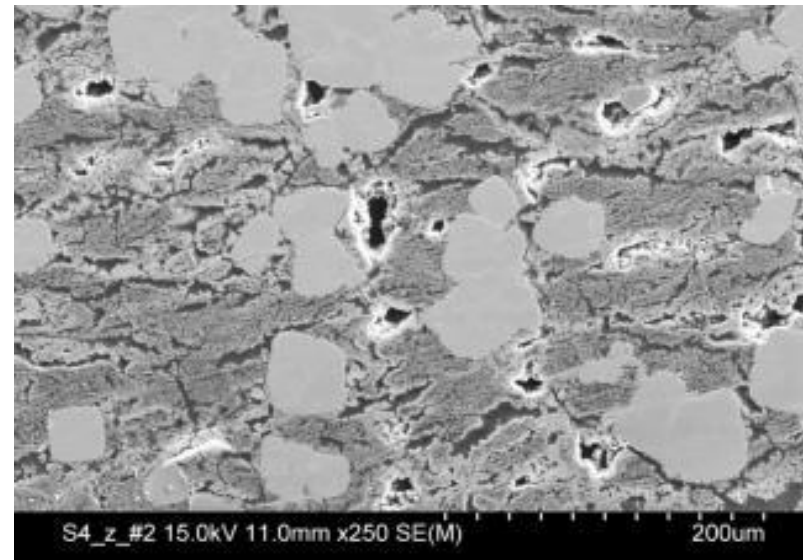
CO_2 exposure - failure/flooding – O_2 exposure – repair - CO_2 exposure



Experiments



Field case



Arne Dugstad, Simona Palencsar, Tonje Berntsen, Linda Børvik "Corrosion of Steel Armour Wires in Flexible Pipes – History Effects", Oilfield Corrosion 2018, SPE-190907-MS

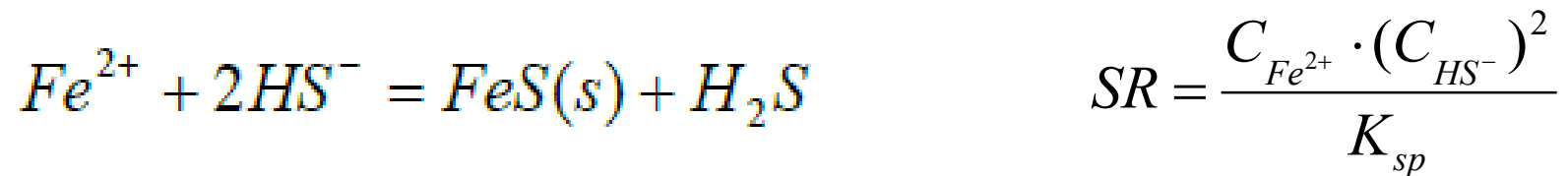
A. Dugstad, S. Palencsár, G. Svenningsen, J. Muren, M. Eriksen, J. Melville, K. Sanghavi, *The combined effect of O₂ and CO₂ on corrosion of flexible armour wires*, CORROSION/2020, paper no. 14790 (NACE International, 2020)

H₂S consumption

- FeS precipitates much faster than FeCO₃ for a given supersaturation.
- Essentially instantaneous reaction: SR_{FeS} about 1 (?)

Consequences:

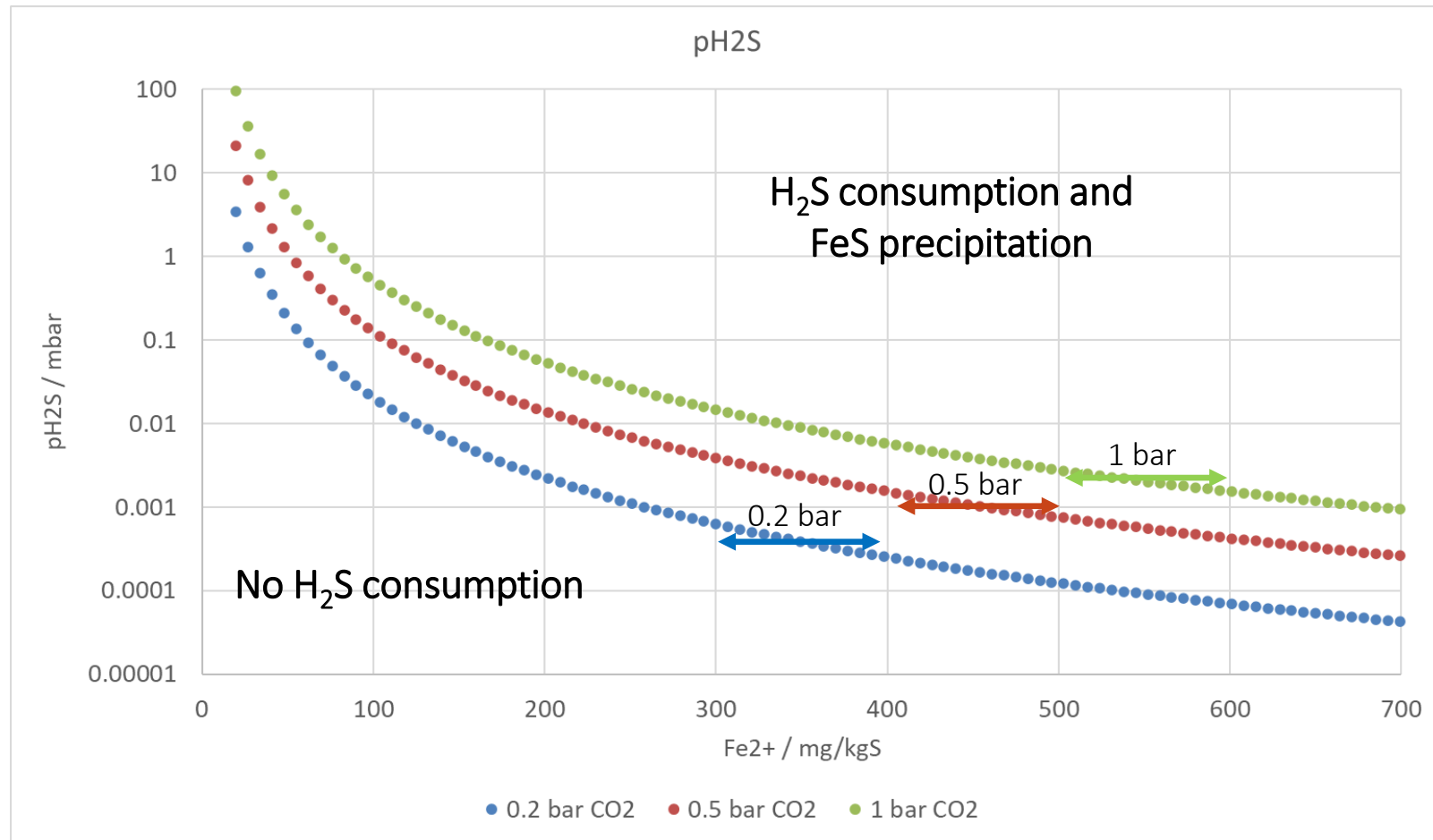
- Precipitation of FeS consumes the added H₂S
- Direct relationship between Fe²⁺ and H₂S concentration



Not possible to have CO₂ controlled corrosion rate and high H₂S content at the same time!

pH_2S assuming equilibrium ($\text{SR}_{\text{FeS}} = 1$)

Temp, pCO_2 , type of water, Fe^{2+} precipitated, Fe^{2+} produced



Summary

- Most flexibles perform as expected, i.e. corrosion rates < 0.01 mm/y, no cracking
- Air ingress, damaged outer sheath and sea water flooding are challenging
 - Oxygen ingress destabilize protective FeCO_3 films and gives higher corrosion rates and pitting
- What is the corrosion rate after repair (history effect)?
- H_2S consumption expected. Very fast precipitation of FeS
- CO_2 consumption reduces the potential corrosion rate
- CO_2 SCC cracking (a new failure mode Brazil 2016) and Fatigue
 - **Residual stress**, surface history/microstructure, steel type and annulus chemistry important
- The annulus chemistry is complex, like a clockwork depending on a large number of time dependent parameters

Issues for
new IFE JIP
KFC-II

Sea water ingress
 O_2 ingress
 Pressure
 Temp
 O_2

